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INCH-POUND
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MS3217C
25 October 2011
SUPERSEDING
MS3217B
14 JULY 1989

## DETAIL SPECIFICATION SHEET

RING, RETAINING, EXTERNAL, HEAVY-DUTY
(TAPERED SECTION TYPE)

This specification is approved for use by all Departments and Agencies of the Department of Defense.
The requirements for acquiring the product described herein shall consist of this specification sheet and procurement specification MIL-R-21248.


FIGURE 1. Ring, Retaining.

## MS3217C

TABLE I. Dimensions.

| $\begin{gathered} \quad \varnothing \mathrm{S} \\ \text { SHAFT } \\ \text { (REF) } \end{gathered}$ |  | $\begin{gathered} \varnothing \mathrm{OD} \\ \text { FREE } \end{gathered}$ |  | $\begin{gathered} \hline \text { B } \\ \text { LUG HEIGHT } \end{gathered}$ |  | E LARGE SECTION HEIGHT |  | SMALL SECTION HEIGHT |  | $\begin{gathered} \mathrm{T} \frac{1}{1} \\ \text { THICKNESS } \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INCH | MM | BASIC | TOL | BASIC | TOL | BASIC | TOL | BASIC | TOL | BASIC | TOL |
| . 394 | 10.0 | . 362 | $\begin{aligned} & \hline+.003 \\ & -.008 \end{aligned}$ | . 101 |  | . 068 | $\pm .004$ | . 039 | $\pm .004$ | . 035 |  |
| . 473 | 12.0 | . 435 |  | . 101 |  | . 088 |  | . 053 |  | . 042 |  |
| . 500 | 12.7 | . 460 |  | . 120 | $\pm .004$ | . 090 |  | . 050 |  | . 050 | $\pm .002$ |
| . 591 | 15.0 | . 543 |  | . 130 |  | . 102 | $\pm .005$ | . 057 | $\pm .005$ | . 050 |  |
| . 625 | 15.9 | . 575 |  | . 130 |  | . 106 |  | . 059 |  | . 050 |  |
| . 669 | 17.0 | . 616 |  | . 130 |  | . 112 |  | . 062 |  | . 050 |  |
| . 750 | 19.0 | . 689 |  | . 180 |  | . 127 |  | . 077 |  | . 078 |  |
| . 787 | 20.0 | . 689 | +. 005 | . 180 |  | . 127 |  | . 077 |  | . 078 |  |
| . 875 | 22.2 | . 804 | -. 010 | . 180 |  | . 148 | $\pm .006$ | . 083 | $\pm .006$ | . 078 |  |
| . 984 | 25.0 | . 906 |  | . 180 |  | . 151 |  | . 084 |  | . 078 |  |
| 1.000 | 25.4 | . 906 |  | . 180 |  | . 151 |  | . 084 |  | . 078 |  |
| 1.062 | 27.0 | . 978 |  | . 220 |  | . 161 |  | . 090 |  | . 093 |  |
| 1.125 | 28.6 | 1.036 |  | . 220 |  | . 169 |  | . 095 |  | . 093 |  |
| 1.181 | 30.0 | 1.087 |  | . 220 |  | . 176 |  | . 098 |  | . 093 |  |
| 1.188 | 30.2 | 1.087 |  | . 220 | $\pm .005$ | . 176 |  | . 098 |  | . 093 |  |
| 1.250 | 31.7 | 1.150 | $\begin{aligned} & +.010 \\ & -.015 \end{aligned}$ | . 220 |  | . 185 | $\pm .007$ | . 103 | $\pm .007$ | . 093 | $\pm .003$ |
| 1.312 | 33.3 | 1.208 |  | . 220 |  | . 192 |  | . 106 |  | . 093 |  |
| 1.375 | 34.9 | 1.268 |  | . 220 |  | . 200 |  | . 110 |  | . 093 |  |
| 1.378 | 35.0 | 1.268 |  | . 220 |  | . 200 |  | . 110 |  | . 093 |  |
| 1.500 | 38.1 | 1.380 |  | . 280 |  | . 218 |  | . 123 |  | . 109 |  |
| 1.562 | 39.7 | 1.437 |  | . 280 |  | . 228 |  | . 127 |  | . 109 |  |
| 1.575 | 40.0 | 1.437 |  | . 280 |  | . 228 |  | . 127 |  | . 109 |  |
| 1.750 | 44.4 | 1.608 | +. 013 | . 290 |  | . 254 | $\pm .008$ | . 140 | $\pm .008$ | . 109 |  |
| 1.772 | 45.0 | 1.608 | -. 020 | . 290 |  | . 254 |  | . 140 |  | . 109 |  |
| 1.938 | 49.2 | 1.782 |  | . 314 |  | . 280 |  | . 154 |  | . 125 |  |
| 1.969 | 50.0 | 1.782 |  | . 314 | $\pm .006$ | . 280 |  | . 154 |  | . 125 | $\pm .004$ |
| 2.000 | 50.8 | 1.840 |  | . 314 |  | . 290 |  | . 160 |  | . 125 |  |

TABLE I. Dimension. (Continued)

| $\begin{gathered} \quad \varnothing \mathrm{S} \\ \text { SHAFT } \\ \text { (REF) } \end{gathered}$ |  | $\varnothing G$ W <br> RECOMMENDED GROOVE (REF)  |  |  |  | бK 3/ <br> MAX | $\begin{aligned} & \hline \varnothing C \text { 4I } \\ & \text { CLEAR } \end{aligned}$ | R $\underline{5} / \mathrm{CH} \underline{5} /$ <br> OF RETAINED <br> PART (REF) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INCH | MM | BASIC | TOL | BASIC | TOL |  |  | MAX | MAX |
| . 394 | 10.0 | . 368 | $\begin{gathered} \hline+.001 \\ -.002 \end{gathered}$ | . 040 | $\begin{aligned} & +.003 \\ & -.000 \end{aligned}$ | . 479 | 61 | . 047 | . 039 |
| . 473 | 12.0 | . 444 | . 002 | . 047 |  | . 589 | . 69 | . 070 | . 058 |
| . 500 | 12.7 | . 468 | FIM 2 / | . 056 | +. 004 | . 613 | . 75 | . 070 | . 058 |
| . 591 | 15.0 | . 555 |  | . 056 | -. 000 | . 719 | . 86 | . 070 | . 058 |
| . 625 | 15.9 | . 588 |  | . 056 |  | . 758 | . 90 | . 074 | . 062 |
| . 669 | 17.0 | . 629 | +. 001 | . 056 |  | . 808 | . 94 | . 077 | . 064 |
| . 750 | 19.0 | . 704 | -. 003 | . 086 |  | . 913 | 1.12 | . 089 | . 074 |
| . 787 | 20.0 | . 740 | . 002 | . 086 |  | . 949 | 1.16 | . 089 | . 074 |
| . 875 | 22.2 | . 821 |  | . 086 |  | 1.056 | 1.25 | . 100 | . 083 |
| . 984 | 25.0 | . 925 | FIM $\underline{2} /$ | . 086 |  | 1.164 | 1.36 | . 100 | . 083 |
| 1.000 | 25.4 | . 938 |  | . 086 |  | 1.177 | 1.37 | . 100 | . 083 |
| 1.062 | 27.0 | . 998 |  | . 103 |  | 1.256 | 1.52 | . 106 | . 088 |
| 1.125 | 28.6 | 1.059 |  | . 103 |  | 1.329 | 1.58 | . 112 | . 093 |
| 1.181 | 30.0 | 1.111 | +. 002 | . 103 |  | 1.391 | 1.64 | . 112 | . 093 |
| 1.188 | 30.2 | 1.111 | $\begin{array}{r} .004 \\ .004 \end{array}$ | . 103 | $\begin{aligned} & +.005 \\ & -.000 \end{aligned}$ | 1.391 | 1.64 | . 112 | . 093 |
| 1.250 | 31.7 | 1.174 |  | . 103 |  | 1.468 | 1.70 | . 112 | . 093 |
| 1.312 | 33.3 | 1. 234 | FIM $\underline{2}^{\prime}$ | . 103 |  | 1.538 | 1.77 | . 128 | . 107 |
| 1.375 | 34.9 | 1.291 |  | . 103 |  | 1.607 | 1.83 | . 128 | . 107 |
| 1.378 | 35.0 | 1.291 |  | . 103 |  | 1.607 | 1.83 | . 128 | . 107 |
| 1.500 | 38.1 | 1.406 |  | . 120 |  | 1.752 | 2.08 | . 128 | . 107 |
| 1.562 | 39.7 | 1.468 | +. 003 | . 120 |  | 1.829 | 2.14 | . 128 | . 107 |
| 1.575 | 40.0 | 1.480 | -. 004 | . 120 |  | 1.841 | 2.15 | . 128 | . 107 |
| 1.750 | 44.4 | 1.650 | . 004 | . 120 |  | 2.050 | 2.34 | . 128 | . 107 |
| 1.772 | 45.0 | 1.669 |  | . 120 |  | 1.069 | 2.37 | . 128 | . 107 |
| 1.938 | 49.2 | 1.826 | FIM $\underline{2} /$ | . 139 |  | 2.265 | 2.58 | . 153 | . 128 |
| $\begin{aligned} & 1.969 \\ & 2.000 \\ & \hline \end{aligned}$ | 50.0 50.8 | $\begin{array}{r} 1.850 \\ 1.880 \\ \hline \end{array}$ |  | $\begin{array}{r} .139 \\ .139 \end{array}$ | $\begin{aligned} & +.006 \\ & -.000 \end{aligned}$ | $\begin{aligned} & 2.289 \\ & 2.334 \\ & \hline \end{aligned}$ | 2.61 2.64 | . 153 | .128 .128 |

1/ $\mathrm{T}=$ Thickness " $T$ " applies to unplated rings. For corrosion resistant steel and plated rings, +.002 should be added to the maximum tolerance, i.e., $\pm .002$ should be +.004/-. 002 .
$\underline{2 /}$ FIM $=($ Full Indicator Movement $)$ is the maximum allowable deviation of concentricity between the groove and the shaft.
3/ $\mathrm{K}=$ Maximum diameter when the ring is properly seated in the groove (design reference dimension).
4/ $\mathrm{C}=$ Actual clearance diameter when the ring is sprung over the shaft prior to installation into the groove (design reference dimension).
5/ R and $\mathrm{CH}=$ Radii or chamfers allowable on parts to be retained by the rings. Thrust loads of rings, retaining parts with corner radii or chamfers (see note "3 (g)" on page 7).

Requirements:

1. Classification: Retaining rings furnished under this standard shall be Type I, Class 10 of the procurement specification, MIL-R-21248.

## 2. Material:

(a) Carbon steel, grade 1060 thru 1095 (UNS G10600 thru G10950) in accordance with ASTM A568/A568M or ASTM A684/A684M.
(b) Corrosion resistant steel in accordance with SAE-AMS 5520 (UNS S15700).
(c) Beryllium copper alloy number 170 (UNS C17000) or alloy number 172(UNS C17200) in accordance with ASTM B194.
3. Hardness:

TABLE II. Hardness.

| $\varnothing$ SHAFT <br> $($ REF $)$ | CARBON STEEL | CORROSION <br> RESISTANT STEEL | BERYLLIUM <br> COPPER |
| :--- | :--- | :--- | :--- |
| .394 to .625 | $67.5-75$ HR30N | $63-69.5$ HR30N | $54-62$ HR30N |
| .669 to 2.000 incl. | $47-52$ HRC | $44-51$ HRC | $34-43$ HRC |

4. Protective finish or surface treatment:
(a) Carbon steel - shall be as specified (see Table III):
(1) Cadmium plate in accordance with SAE-AMS-QQ-P-416, Type II, Class 3 or ASTM B696, Type II, Class 5.
(2) Zinc coat in accordance with ASTM B633, Type II, Class Fe/Zn5, or ASTM B695, Type II, Class 5.
(3) Phosphate coating accordance with MIL-DTL-16232, Type Z, Class 2.
(b) Corrosion resistant steel - shall be cleaned, descaled and passivated in accordance with SAEAMS2700.
5. Part number: The basic MS part number is followed by a dash number taken from Table III.

Example: MS3217-1200 is the part number for a carbon steel, cadmium plate, external, heavy duty retaining ring for use on a 2.000 diameter shaft.

TABLE III. Dash numbers for MS3217

| $\begin{gathered} \quad \varnothing \mathrm{S} \\ \text { SHAFT } \\ \text { (REF) } \end{gathered}$ | CARBON STEEL 1/ CADMIUM PLATE | CARBON STEEL 1/ ZINC COAT | CARBON STEEL 1/ PHOSPHATE COAT | $\begin{gathered} \text { STEEL, } \\ \text { CORROSION } \\ \text { RESISTANT } \end{gathered}$ | $\underset{\text { COPPER }}{\text { BERYLLIUM }}$ 1/ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | DASH NO. | DASH NO. | DASH NO. | DASH NO. | DASH NO. |
| . 394 | -1039 | -2039 | -3039 | -4039 | -5039 |
| . 473 | -1047 | -2047 | -3047 | -4047 | -5047 |
| . 500 | -1050 | -2050 | -3050 | -4050 | -5050 |
| . 591 | -1059 | -2059 | -3059 | -4059 | -5059 |
| . 625 | -1062 | -2062 | -3062 | -4062 | -5062 |
| . 669 | -1066 | -2066 | -3066 | -4066 | -5066 |
| . 750 | -1075 2/ | -2075 21 | -3075 2/ | -4075 2/ | -5075 2/ |
| . 787 | -1075 ${ }^{\text {2/ }}$ | -2075 ${ }^{\text {2/ }}$ | -3075 ${ }^{\text {2/ }}$ / | -4075 ${ }^{2} /$ | -5075 ${ }^{\underline{2} /}$ |
| . 875 | -1087 | -2087 | -3087 | -4087 | -5087 |
| . 984 | -1098 2/ | -2098 21 | -3098 21 | -4098 21 | -5098 21 |
| 1.000 | -1098 21 | -2098 21 | -3098 21 | -4098 21 | -5098 21 |
| 1.062 | -1106 | -2106 | -3106 | -4106 | -5106 |
| 1.125 | -1112 | -2112 | -3112 | -4112 | -5112 |
| 1.181 | -1118 $\underline{2}^{1}$ | -2118 ${ }^{\text {2 }}$ | -3118 $\underline{2}^{\prime}$ | -4118 ${ }^{\text {2 }}$ | -5118 $\underline{2 l}^{\prime}$ |
| 1.188 | -1118 $\underline{2}^{\prime}$ | -2118 ${ }^{\text {2 }}$ | -3118 $\underline{2}^{\prime}$ | -4118 ${ }^{\underline{2} /}$ | -5118 ${ }^{\underline{2} /}$ |
| 1.250 | -1125 | -2125 | -3125 | -4125 | -5125 |
| 1.312 | -1131 | -2131 | -3131 | -4131 | -5131 |
| 1.375 | -1137 2/ | -2137 2/ | -3137 2/ | -4137 21 | -5137 2/ |
| 1.378 | -1137 ${ }^{\text {2/ }}$ | -2137 ${ }^{\text {2/ }}$ | -3137 ${ }^{\text {2/ }}$ | -4137 ${ }^{2} /$ | -5137 ${ }^{\underline{2} /}$ |
| 1.500 | -1150 | -2150 | -3150 | -4150 | -5150 |
| 1.562 | -1156 2 / | -2156 2 / | -3156 21 | -4156 2 / | -5156 2/ |
| 1.575 | $-1156$ | -2156 ${ }^{\underline{2}}$ | -3156 ${ }^{\text {2 }}$ | -4156 $\frac{2}{2} /$ | -5156 ${ }^{2}$ |
| 1.750 | -1175 | -2175 | -3175 ${ }^{2}$ | -4175 ${ }^{2}$ | -5175 ${ }^{2}$ |
| 1.772 | -1175 2/ | -2175 $\underline{2}^{\prime}$ | -3175 ${ }^{\text {2/ }}$ | -4175 ${ }^{\underline{2}}$ | -5175 ${ }^{\underline{2} /}$ |
| 1.938 | -1193 21 | -2193 21 | -3193 21 | -4193 21 | -5193 21 |
| 1968 | -1193 21 | -2193 ${ }^{\text {2 }}$ / | -3193 21 | -4193 ${ }^{\text {2/ } /}$ | -5193 ${ }^{\underline{2} /}$ |
| 2.000 | -1200 | -2200 | -3200 | -4200 | -5200 |

1/ Substitute corrosion resistant steel when used in food processing machinery, or in fuel or lubrication systems, or when used at temperatures over $450^{\circ} \mathrm{F}\left(233^{\circ} \mathrm{C}\right)$
$\underline{2 /}$ Same dash numbers suitable for either shaft diameter (inches or mm)

Notes:

1. Unless otherwise specified, all dimensions in inches.
2. In the event of a conflict between the text of this standard and the references cited herein, the text of this standard shall take precedence.
3. Recommended design limitations and usage:
(a) Intended use - To provide large shoulders for positioning and retaining machine components under heavy loading conditions on shafts, even if components to be secured have large corner radii or chamfers abutting the rings. They withstand comparatively heavy shock loads and high rotational speeds. They eliminate the need for separate thrustwashers. The use of the following formulas are based on the fact that the ring will not fail in compression.

Limitation on use - the following formulas are not to be used for brittle materials such as cast iron, etc.

Warning - Rings shall not be over expanded during installation since this will lead to ring failure. If ring has play between the groove diameter and the inside ring diameter, this indicates that the ring has been over expanded, (providing groove has been machined to recommended dimensions).

For approximate safety RPM limits see Table IV.
TABLE IV. Calculated RPM limits. Apply required safety factor.

| Ø SHAFT (INCHES) |  | . 394 | . 437 | . 500 | . 750 | 1.000 | 1.250 | 1.500 | 1.750 | 2.000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CARBON STEEL AND CORROSION <br> RESISTANT STEEL | RPM <br> LIMIT | 80,000 | 69,000 | 65,000 | 40,000 | 30,000 | 23,000 | 18,500 | 15,500 | 14,000 |
| BERYLLIUM COPPER | RPM <br> LIMIT | 51,000 | 44,000 | 41,000 | 26,000 | 19,000 | 14,500 | 12,000 | 10,000 | 9,000 |

(b) Allowable thrust load capacity of the ring. Abutting components to have sharp corners $=$

> P = Allowable thrust load (Pounds)
> S = Shaft diameter (Inches)
> $P=\frac{C_{f} \Pi S T X}{F}$
> Where: $\quad T=$ Ring thickness (Inches)
> $X=$ Ultimate shear strength of the ring material (PSI) 1/
> $F=$ Factor of safety, $F=4$ is recommended to insure $\bar{a}$ safe working load
> $C_{f}=$ Conversion factor, $C_{F}=1.3$ is required since thicker rings increase safety of assembly
(c) Allowable load capacity of groove wall =

P = Allowable compression load (Pounds)
S = Shaft diameter (Inches)

$$
P=\frac{C_{f} \pi S d Y}{F}
$$

Where: $\quad d=$ Groove depth (Inches)
$\mathrm{Y}=$ Yield strength in compression of the groove material (PSI)
$F=$ Factor of safety, $F=2$ is recommended to insure a safe working load
$C_{f}=$ Conversion factor, $C_{F}=2$ is required since contact area in groove is increased due to thicker ring
(d) Minimum distance between outer groove wall and end of shaft $=$

$$
\begin{array}{ll}
Z=3 d \quad \text { Where: } \quad Z=\text { Minimum distance between outer groove and end of } \\
\text { shaft (Inches) } \\
d=\text { Groove depth (Inches) }
\end{array}
$$

(e) Allowable shaft diameter $=$

$$
S=\sqrt{G^{2}+\frac{4 F P}{Y \pi C_{f}}}
$$

$$
\begin{array}{ll}
\text { S }=\text { Allowable shaft diameter } \\
\mathrm{G}=\text { Groove depth } \\
\text { Where: } & \mathrm{F}=\text { Factor of safety (see formula (c) above) } \\
\mathrm{P}=\text { Design load } \\
\mathrm{Y}=\text { Yield strength in compression of the groove material (PSI) } \\
& \mathrm{C}_{\mathrm{f}}=\text { Conversion factor (see formula (c) above) }
\end{array}
$$

(f) Differential rotation $=$

The condition under which a retaining ring may be used when adjacent parts rotate relative to it, fall into two categories:
(1) Where no thrust is exerted by adjacent part. In this case, differential rotation of ring and adjacent part creates no element of risk in the application of the rings because no frictional torque is exerted by the machine part on the ring.
(2) Consideration must be given to the magnitude of the thrust involved. The friction moment may not exceed the bending moment, which the ring can tolerate without releasing its pressure against the bottom of the groove, formulated as follows:

$$
\begin{aligned}
& \mathrm{fPN} \leq \frac{\mathrm{sTE}^{2}}{18} \text { or } \\
& \mathrm{P}=\text { Allowable thrust load exerted by adjacent part (Pounds) } \\
& \mathrm{f}=\text { Coefficient of friction } \\
& \mathrm{s}=\text { Working stress of ring under maximum expansion (PSI) } \underline{2} / \\
& \text { Where: } \quad \mathrm{T}=\text { Ring thickness (Inches) } \\
& P \leq \frac{s T E^{2}}{F 18 N} \\
& \mathrm{E}=\mathrm{Greatest} \text { width section of ring (Inches) } \\
& \mathrm{N}=\text { Neutral ring diameter (Inches) }=\text { free diameter plus 3/4 } \\
& \text { E dimension }
\end{aligned}
$$

In such cases where differential rotation occurs, the calculation should be based on the MAXIMUM possible value of the coefficient of friction.

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(g) Impact capacity of ring and groove wall =

$$
\begin{aligned}
& \mathrm{IR}=\frac{\mathrm{PT}}{2} \quad \text { - For the ring (Inch Pounds) Abutting components to have sharp corners } \\
& \mathrm{IG}_{\mathrm{G}}=\frac{\mathrm{Pd}}{2} \quad \text { - For the groove (Inch Pounds) } \\
& \begin{aligned}
\mathrm{P} & =\text {. Allowable thrust load of rings or grooves (Pounds) } \\
\mathrm{T} & =\text { Ring thickness (Inches) } \\
\mathrm{IR} & =\text { Impact capacity of ring (Inch Pounds) } \\
\mathrm{IG} & =\text { Impact capacity of groove wall (Inch Pounds) } \\
\mathrm{d} & =\text { Groove depth (Inches) }
\end{aligned}
\end{aligned}
$$

1/ $X=150,000$ PSI ultimate shear strength for rings of carbon steel or corrosion resistant steel.
$X=110,000 \mathrm{PSI}$ ultimate shear strength for rings of beryllium copper.
$\underline{2} / \mathrm{s}=250,000 \mathrm{PSI}$ working stress for rings of carbon steel or corrosion resistant steel.
$s=180,000 \mathrm{PSI}$ working stress for rings of beryllium copper.
(h) Load capacity with the retained part radiused or chamfered = when the radius or chamfer of the retained part does not exceed the maximum radius allowed for the bottom of the ring groove, the lesser load capacity computed from the formals on pages 5 and 7 will apply. The corner radii and chamfers listed on page 1 were chosen as large as possible for the ring sizes involved and are related to the maximum thrust loads listed in the table below. If the corner radii or chamfers are smaller than those listed, then the thrust loads increase proportionally, in accordance with the following formulas:

$$
\begin{array}{lll}
P^{1}=\frac{P R}{R^{1}} & P^{1}=\text { New allowable thrust load } \\
& P^{1}=\text { Listed allowable thrust load } \\
P^{1}=\frac{P C h}{C^{1}} & \text { Where: } & R^{1}=\text { New (smaller) corner radius } \\
& R=\text { Listed corner radius } \\
& C^{1}=\text { New (smaller) chamfer } \\
& C h=\text { Listed chamfers }
\end{array}
$$

Limit loads listed in Table V are based on rings of carbon steel or corrosion resistant steel (working stress $250,000 \mathrm{PSI}$ ) and of rings of beryllium copper (working stress $=180,000 \mathrm{PSI}$ ) if the allowable groove capacity loads as calculated by using the formula on page 5 are less, then they should be used.

Table V. Limit loads

| $\varnothing$ Ø <br> Shaft <br> (Ref) |  | Allowable thrust load for ring assemblies with parts having maximum corner radii or chamfers |  |
| :---: | :---: | :---: | :---: |
| From | To | Carbon steel or CRES | Beryllium copper |
| ---- | . 394 | 450 LB | 300 LB |
| ---- | . 473 | 550 LB | 400 LB |
| ---- | . 500 | 650 LB | 450 LB |
| . 591 | . 625 | 750 LB | 550 LB |
| ---- | . 669 | 900 LB | 650 LB |
| . 750 | 1.000 | 2500 LB | 1800 LB |
| 1.062 | 1.378 | 4000 LB | 2900 LB |
| 1.500 | 1.772 | 5000 LB | 3600 LB |
| 1.938 | 2.000 | 6000 LB | 4300 LB |

4. Changes from previous issue. Marginal notations are not used in this revision to identify changes with respect to the previous issue due to the extent of the changes.

## MILITARY INTEREST

| Custodians: | Preparing activity: |
| :--- | :---: |
| Army - AR | DLA - IS |
| Navy - OS | (Project $5325-2011$-004) |

NOTE: The activities listed above were interested in this document as of the date of this document. Since organizations and responsibilities can change, you should verify the currency of the information above using the ASSIST Online database at https://assist.daps.dla.mil

