FED-STD-H28/2A 20 April 1984 SUPERSEDING FED-STD-H28/2 FED-STD-H28/3 31 March 1978 (See Note)

# FEDERAL STANDARD SCREW - THREAD STANDARDS FOR FEDERAL SERVICES SECTION 2 UNIFIED INCH SCREW THREADS— UN AND UNR THREAD FORMS

This standard was approved by the Assistant Administrator, Office of Federal Supply and Services, General Services Administration, for the use of all Federal Agencies.

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NO DELIVERABLE DATA REQUIRED BY THIS DOCUMENT

THDS

#### INFORMATION SHEET ON FEDERAL STANDARDS

This Federal Standard is issued in loose-leaf form to permit the insertion or removal of new or revised pages and sections.

All users of Federal Standards should keep them up to date by inserting revised or new pages as issued and removing superseded and canceled pages.

New and revised pages will be issued under Change Notices which will be numbered consecutively and will bear the date of issuance. Change Notices should be retained and filed in front of the standard until such time as they are superseded by a reissue of the entire standard.

#### FOREWORD

This section was developed to provide Unified Inch Screw Threads for the Federal Services. It was formerly known as "Unified Thread Form and Thread Series for Bolts, Screws, Nuts, Tapped Holes and General Applications". The present issue is a complete revision of FED-STD-H28/2 dated 31 March 1978. It also includes the material previously identified as FED-STD-H28/3 dated 31 March 1978, which was known as "Unified Threads of Special Diameters, Pitches, and Lengths of Engagement". Material from Appendices A3 and A5 of FED-STD-H28 dated 31 March 1978 has been revised and is now in Appendices A and B, respectively, of FED-STD-H28/2A.

FED-STD-H28/2A was prepared by the Defense Industrial Supply Center (DLA-IS) and incorporates the American National Standard for Unified Inch Screw Threads, ANSI P1.1-1982. Significant changes from the previous issues include the following:

- (1) Added UNR, external thread form with mandatory rounded root.
- (2) Revised tolerance requirements for lead and flank angles.
- (3) Added requirements for control of surface texture, chamfers, and rolled thread lead-ins and run-outs.
- (4) Added requirement that inspection methods for acceptability are in accordance with FED-STD-H28/20.

#### SECTION 2 - Unified Inch Screw Threads -UN and UNR Thread Forms

1. <u>Scope</u>. This section provides the standard for unified inch screw threads to be used by the Federal Services.

1.1 Limitations. Only UN and UNR screw threads are covered in this section. For UNJ threads (controlled external thread root with rounded form and increased form minor diameter) see FED-STD-H28/4 (MIL-S-8879). For UNM threads (miniature threads) see FED-STD-H28/5.

1.2 Application.

1.2.1 UN form screw threads. The UN thread is intended for general purpose fastening applications. Its external thread root may be either flat or rounded.

1.2.2 UNR form screw threads. The UNR form applies only to external threads. Its design form is the same as that of the external UN thread except that the root is required to be rounded. UNR threads are applied most often to high volume commercial fastener threads produced by rolling.

NOTE: The mandatory rounded root of the UNR thread greatly reduces the concentration of stress, hence increases the fatigue life of threaded parts.

2. Referenced documents.

2.1 <u>Government publications</u>. The issues of the following documents in effect on the date of invitation for bids or request for proposal form a part of this standard to the extent specified herein.

Federal standards.

- FED-STD-H28/1 Nomenclature, Definitions and Letter Symbols for Screw Threads
- FED-STD-H28/6 Gages and Gaging for Unified Screw Threads
- FED-STD-H28/20 Inspection Methods for Acceptability of UN, UNR, UNJ, M and MJ Screw-Threads

(Activities outside the Federal Government may obtain copies of Federal specifications, standards, and commercial item descriptions as outlined under General Information in the Index of Federal Specifications, Standards, and Commercial Item Descriptions. The Index, which includes cumulative bi-monthly supplements as issued, is for sale on a subscription basis by the Superintendent of Documents, U.S. Government Printing Office, Washington, DC 20402.

(Single copies of this specification and other Federal specifications and commercial item descriptions required by activities outside the Federal Government for bidding purposes are available without charge from General Services Administration Business Service Centers in Boston, MA; New York, NY; Philadelphia, PA; Washington, DC; Atlanta, GA; Chicago, IL; Kansas City, MO; Fort Worth, TX; Houston, TX; Denver, CO; San Francisco, CA; Los Angeles, CA; and Seattle, WA.

(Federal Government activities may obtain copies of Federal standardization documents, and the Index of Federal Specifications, Standards, and Commercial Item Descriptions from established distribution points in their agencies.)

2.2 Other publications. The following documents form a part of this standard to the extent specified herein. Unless a specific issue is identified, the issue in effect on date of invitation for bids or request for proposal shall apply.

#### American National Standards.

ANSI B1.1-1982 Unified Inch Screw Threads (UN and UNR Thread Form)

ANSI B46.1 Surface Texture - Surface Roughness, Waviness and Lay

(Application for copies should be addressed to the American Society of Mechanical Engineers, United Engineering Center, 345 East 47th Street, New York, NY 10017 or the American National Standards Institute, 1430 Broadway, New York, NY 10018.)

3. Definitions. The terms applicable to this standard are defined in FED-STD-H28/1.

4. General requirements.

4.1 Screw threads. Unified inch screw threads shall be in accordance with ANSI B1.1-1982 and this Federal Standard. Only Standard Series Unified Screw Threads, listed in Table 3A of ANSI B1.1-1982, shall be used for new design for the Federal Services unless prior approval has been granted by the procurement authority to deviate from them. Coarse and fine thread series are preferred.

4.2 <u>Acceptability</u>. Screw thread inspection methods for acceptability shall be in accordance with FED-STD-H28/20. The required gaging system shall be specified in accordance with that standard.

4.3 Gages and gaging. Gages and gaging shall be in accordance with FED-STD-H28/6.

#### 5. Detailed requirements.

5.1 <u>Diameter-pitch combinations</u>. When standard size screw threads referred to in 4.1 cannot be used, the designer should choose preferred sizes of special threads listed in Table 3B of ANSI B1.1-1982. If this is not possible, consideration should be given to the following sub-paragraphs in the choice of thread.

5.1.1 Preferred non-standard diameters. Whenever possible, the nominal diameter should be selected from series of diameter increments as follows:

Diameter range	First choice increment	Second choice increment
inch	inch	inch
0.25 to 0.6 above 0.6 to 1.5 above 1.5 to 6.0 above 6 to 16 above 16 to 24	0.05 0.1 0.25 0.5 1.0	0.05 0.1 0.25 0.5

It is recommended that diameters less than 0.25 inch conform to the standard sizes as there is virtually no necessity for the selection of a diameter not included in those sizes. Also, the coarse and fine thread series provide ample choice of diameter-pitch combinations.

5.1.2 Preferred non-standard pitches. Whenever possible, the pitch should be selected from one of the following; 40, 36, 32, 28, 24, 20, 16, 12, 10, 8, 6 and 4 threads per inch. Intermediate pitches should be used only when absolutely necessary. Pitches coarser than 4 threads per inch are not recommended. The curves shown in Figure 2.B.2 of Appendix B cover the practical diameter limits suggested for each pitch.

5.2 <u>Thread Class Selection</u>. Standard Unified thread classes and their applications are described in Section 4 of ANSI B1.1-1982. When selecting a thread class, consideration should first be given to the use of a class 2A external thread with a class 2B internal thread since these classes are designed for general use. Before specifying class 3A/3B series, it must be considered whether the additional production cost, necessary for the tighter fit and tolerance is justified. If a fit looser than the standard class 1A/1B is required, the non-preferred class 1AR may be specified for an external thread of 16 threads per inch and coarser. This special class 1 thread with the Unified class 1A thread tolerance. See 5.2.2 for class 1AR allowance.



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5.2.1 <u>Replacements for obsolete American National thread classes</u>. When threads specified with the obsolete American National thread classes are to be replaced by unified threads, the following guidelines are provided:

- a. American National class 1 coarse thread series (NC-1) is approximately equivalent to Unified class 1A/1B series. Class 1 fine thread series (NF-1) is approximately equivalent dimensionally to Unified class 2A/2B series. Standard Unified series threads should be considered prior to approval of replacement by non-standard threads
- b. American National class 2 coarse thread series (NC-2), 8 thread series (8N-2), 12 thread series (12N-2), 16 thread series (16N-2), and extra fine thread series (NEF-2) are most nearly equivalent to Unified series UNC-2A/2B, 8UN-2A/2B, 12UN-2A/2B, 16UN-2A/2B and UNEF-2A/2B respectively. Class 2 fine thread series (NF-2) is approximately equivalent dimensionally to Unified class 3A/3B series, but the use of class 2A/2B series should be considered prior to approval of replacement by class 3A/3B.
- c. American National class 3 series NC-3, NF-3, NEF-3, 8N-3, 12N-3 and 16N-3 are most nearly equivalent to Unified class 3 series UNC-3A/3B, UNF-3A/3B, UNEF-3A/3B, 8UN-3A/3B, 12UN-3A/3B and 16UN-3A/3B, respectively.
- d. There is no Unified thread class equivalent to the old American National class 4 which required selective fit of parts due to the possibility of interference.

5.2.2 Thread allowance and tolerance. Allowances and tolerances specified for standard Unified thread classes are described in Section 5 of ANSI B1.1-1982. For the special external thread class 1AR, tolerances are the same as for class 1A and allowances are as follows:

Threads per inch	Class 1AR allowance
16 14 12 10 8 6 4	inch 0.0018 0.0021 0.0024 0.0028 0.0034 0.0034 0.0044 0.0064

To complement paragraph 5.6 of ANSI B1.1-1982, recommended tap drill sizes and hole size limits before threading, for different lengths of engagement, are included in Appendix A.

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5.3 <u>Designation</u>. Designation of Unified screw threads is in accordance with section 6 of ANSI B1.1-1982. Nominal size shall be stated in decimals. The symbol UNS is applicable to any thread:

- (1) having the basic Unified thread form
- (2) with limits based upon Unified formulations, and
- (3) which is not in the standard series listed in Table 3A of ANSI B1.1-1982.

5.4 Limits of size. See section 8 of ANSI B1.1-1982 for limits of size of standard and preferred non-standard threads and for information used for calculation of non-standard thread size limits which are not tabulated. For class 1AR, calculate as for class 1A except allowance is tabulated in 5.2.2. The following example illustrates the procedure necessary to calculate the limits of size of a non-standard thread; this follows the outlines in tables 1A and 1B of ANSI B1.1-1982:

External thread, 2.500 - 28UNS-2A Length of engagement, 1 inch Maximum major diameter = Nominal size - allowance (section 13 of ANSI B1.1-1982) = 2.5000 - 0.0014 (from table 32 of ANSI B1.1-1982) = 2.4986Minimum major diameter = Maximum major diameter - tolerance (Section 13 of ANSI B1.1-1982) = 2.4986 - 0.0065 (from table 31 of ANSI B1.1-1982) = 2.4921 Maximum pitch diameter = Maximum major diameter - h<sub>b</sub> (table 6, col. 13 of ANSI B1.1-1982) = 2.4986 - 0.0232 (rounded from 0.023197) = 2.4754Minimum pitch diameter = Maximum pitch diameter - tolerance (section 13 of ANSI B1.1-1982) = 2.4754 - 0.0056 (from table 34 of ANSI B1.1-1982) = 2.4698Nominal (maximum) minor = Maximum major diameter - 2h<sub>n</sub> diameter (table 6, col. 15 of ANSI B1.1-1982) = 2.4986 - 0.0387 (rounded from 0.03866) = 2.4599

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Internal thread 2.500 - 28UNS-2B (to mate with the above thread)

Minimum minor diameter = Nominal size -  $2h_n$ (table 6, col. 15 of ANSI B1.1-1982) = 2.5000 - 0.0387 (rounded from 0.03866) = 2.4613 which is rounded to 2.461

Maximum minor diameter = Minimum minor diameter + tolerance (section 13 of ANSI B1.1-1982). = 2.4613 + 0.0063 (from table 39 of ANSI B1.1-1982 for length of engagement of 0.4D) = 2.4676 which is rounded to 2.468

Minimum pitch diameter = Nominal size -  $h_b$ (table 6, col. 13 of ANSI B1.1-1982) = 2.5000 - 0.0232 (rounded from 0.023197) = 2.4768

Maximum pitch diameter = Minimum pitch diameter + tolerance (section 13 of ANSI B1.1-1982) = 2.4768 + 0.0073 (from table 37 of ANSI B1.1-1982) = 2.4841

Nominal (minimum) major = Nominal size 1 N 63 diameter

= 2.5000

Factors used in the design of threads, particularly special threads, are presented in Appendix B. It is to be noted that deviations from standard tolerances for major diameter of the external thread and for minor diameter of internal thread may be necessary in order to arrive at the optimum design.

5.5 Surface texture.

5.5.1 The threads shall have a smooth finish and be free from flaws and other defects, such as fins, nicks and burrs, that would make them unsuitable for the purpose intended.

5.5.2 Workmanship shall be consistent with the tolerances specified herein. Surface texture of threads produced to this standard shall not exceed 100 microinch arithmetical average roughness (Ra) for cut threads and 63 microinch (R) for rolled and ground threads in accordance with ANSI B46.1.

NOTE: Coarse and fine pitch threads with rough surface texture are more likely to cross-thread. Threads with chamfered entering ends have the least tendency to cross-thread when assembled with power tools.

#### 5.6 Chamfer.

5.6.1 All entering ends of fasteners and threaded components shall have 45° chamfers (approximately) from minor diameter of external threads and major diameter of internal threads, unless otherwise specified.

5.7 Rolled threads.

5.7.1 Completely formed threads. A completely formed thread follows the thread profile, within the tolerance zone over an axial distance of one pitch. See figure 2.1.

#### 5.7.2 Incomplete formed threads.

5.7.2.1 The lead-in thread is measured from the end of the product to the start of the first complete thread where the major diameter is equal to the minimum allowable major diameter and the thread root is equal to the maximum minor diameter. This should not exceed 2P. See figure 2.2.

5.7.2.2 The run-out thread is measured between the transition point of the product and the first thread root which is completely formed, where the minor diameter equals the maximum permissible minor diameter and the major diameter of the last fully formed thread equals the minimum permissible major diameter. When root radius is specified, the last completely formed root at the minor diameter must meet the requirement. See figure 2.3 for full shank fastener, figure 2.4 for pitch diameter shank fastener, figure 2.5 for shoulder bolt, figure 2.6 for oversize diameter shank fastener and figures 2.7 and 2.8 for threaded to head fasteners.

6. Notes.

6.1 Supersession note. In addition to superseding FED-STD-H28/2 dated 31 March 1978 and FED-STD-H28/3 dated 31 March 1978, this document also supersedes Appendices A3 and A5 of FED-STD-H28 dated 31 March 1978.

MILITARY INTERESTS:

#### CIVIL AGENCY COORDINATING ACTIVITY:

Custodians

Army - AR Navy - AS Air Force - 11

Review Activities

Army - CR.FA.ER.ME Air Force -15,99

GSA-FSS

PREPARING ACTIVITY: DLA-IS

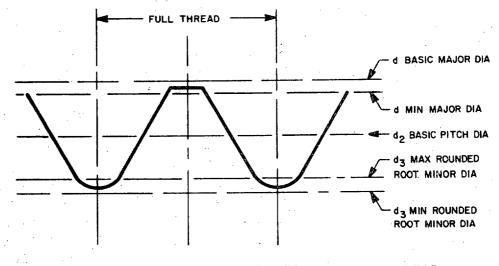
User Activities

Army - AT, MI

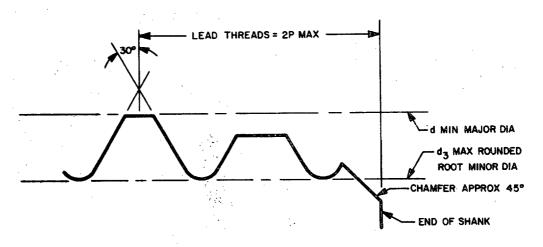
(DoD Project THDS-0044)

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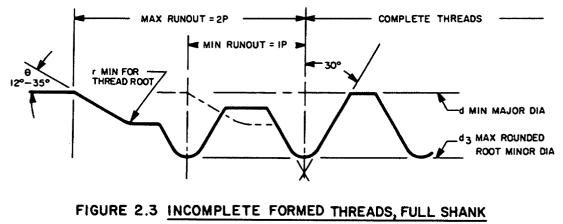
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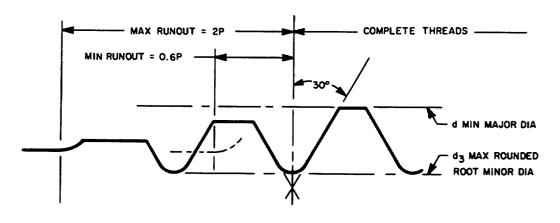
## FIGURE 2.1 COMPLETELY FORMED EXTERNAL THREAD



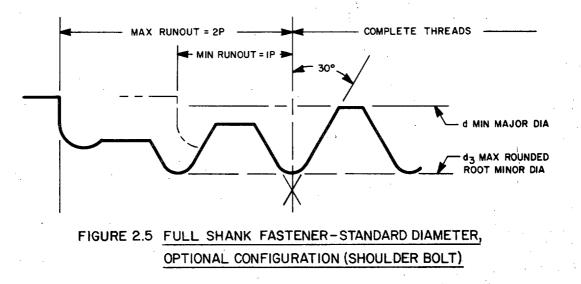
## FIGURE 2.2 INCOMPLETE FORMED EXTERNAL THREADS, LEAD-IN THREADS

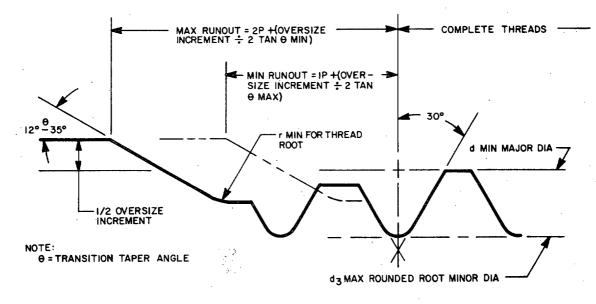


FASTENER-STANDARD DIAMETER









#### FIGURE 2.6 FULL SHANK FASTENER-OVERSIZE DIAMETER

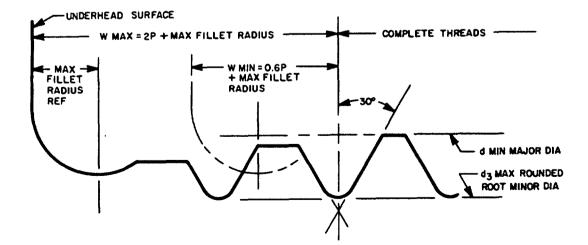
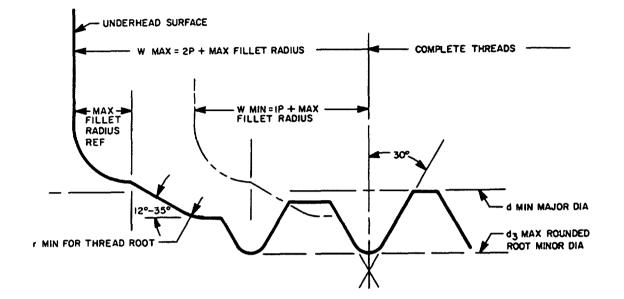


FIGURE 2.7 FULL SHANK FASTENER - THREADED TO HEAD



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#### APPENDIX A

#### TAP DRILL SIZES AND RECOMMENDED HOLE SIZE LIMITS BEFORE THREADING

10. <u>Scope</u>. This appendix provides suggested tap drill sizes and recommended hole size limits applicable prior to forming internal Unified screw threads. It is not a mandatory part of the standard. The information contained herein is intended for guidance only.

20. Tap drill sizes.

20.1 General. To assure that the minor diameter of an internal thread is held within specified limits, it may be necessary to use a reamer to finish the hole. A variety of factors enters into the production of a clean, round, straight hole of the correct diameter. For a discussion of these and other data on drilling and tapping, reference may be made to "Drilled Holes for Tapping", a publication of the Metal Cutting Tool Institute, 1230 Keith Building, Cleveland, OH 44115.

#### 20.2 Tabulated data.

20.2.1 Table II.A.1 gives minor diameter limits and corresponding percentages of thread for all standard series threads up to and including 3.75 inch diameter for classes 1B and 2B. Table II.A.2 is a similar table for class 3B. These tables also list sizes of drills that may be expected to drill holes within or near the specified minor diameter limits. The diameter of the drill, the probable hole size, and the corresponding percentages of thread are tabulated.

20.2.2 As a drill may normally be expected to cut oversize, probable hole sizes are tabulated that are derived from probable mean oversizes, also tabulated. The following is quoted from the above-mentioned report: "... a series of tests was conducted by drill manufacturers. Using six sizes of drills ranging from 1/16" to 1" in diameter, a total of 2,808 holes were drilled in cast iron and steel. Regular high speed steel drills were used with drilling equipment of the type normally found in metal working shops.... The average depth of hole drilled was equal to 1 1/2 times the drill diameter. Measurement of the hole was made at midpoint of the depth drilled....The average of the...amounts oversize...shows a marked increase in amount oversize for drills larger than 3/4". For this size range reaming is recommended."

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20.2.3 Percent of thread listed in tables is the ratio in percent of the actual height of thread to the value 0.75H; this value is the basic thread height of the obsolete American National Thread Profile. Since the basic height of a Unified Thread Profile is 0.625H, the maximum percent thread permissible is 83.3%. Due to allowances for drills to cut oversize or due to lack of availability of drills within specified minor diameter limits, tap drills listed in tables II.A.1 and II.A.2 may show greater than 83.3% threads. This indicates that the drill size is smaller than the minimum thread minor diameter and additional machining of the hole may be necessary in order to permit economical tapping.

30. Recommended hole size limits before threading.

30.1 General. For short length of engagement, the hole diameter required prior to threading should be held near the minimum limit to maximize thread height for maximum joint strength. As length of engagement increases, it is advantageous to increase the hole diameter for more economical tapping with less risk of tap breakage. Therefore, the following recommendations were developed (also see 30.2 below):

Length of Engagement	Minimum Hole Size	Maximum Hole Size
Up to and including 0.33D	Minimum minor dia	Min minor dia plus 1/2 minor dia tolerance
Above 0.33D thru 0.67D	Min minor dia plus 1/4 minor dia tolerance	Min minor dia plus 3/4 minor dia tolerance
Above 0.67D thru 1.5D	Min minor dia plus 1/2 Minor dia tolerance	Max minor dia (min minor dia plus tolerance)
Above 1.5D thru 3.0D	Min minor dia plus 3/4 minor dia tolerance	Max minor dia plus 1/4 minor dia tolerance (See 30.2)

From the foregoing it will be seen that the difference between limits in each range is the same and equal to half of the minor diameter tolerance. This is a general rule. However, the minimum differences for sizes below 0.25 in are equal to the minor diameter tolerances given in tables 39 and 40 in ANSI B1.1-1982 for lengths of engagement to and including 0.33D. For lengths of engagement greater than 0.33D for sizes 0.25 in and larger, the minimum values are adjusted so that the difference between limits is never less than 0.0040 in.



30.2 <u>Tabulated data</u>. Recommended hole size limits for standard Unified threads and some special (UNS) threads are given in tables II.A.3 and II.A.4. For other special threads, calculate in accordance with 30.1 above; use minimum minor diameter and tolerance from table 3B of ANSI B1.1-1982, or calculate in accordance with section 8 of ANSI B1.1-1982 using appropriate tolerance from table 39 or 40 of ANSI B1.1-1982 for tolerance ratio of 1 or from formulas in paragraph 5.8.2 of ANSI B1.1-1982. Tabulated hole sizes and hole sizes calculated in accordance with 30.1 are not mandatory unless the thread designation states the modified minor diameter limits and the designation MOD in accordance with paragraph 6.7 in ANSI B1.1-1982. If modified minor diameter limits are not specified, acceptance will be in accordance with standard minor diameter limits.

NOTE: Recommended maximum hole sizes in 30.1, for lengths of engagement greater than 1.5D are outside standard minor diameter limits. They are not included in tables II.A.3 and II.A.4. Use of a minor diameter larger than standard will result in a reduction in shear area of the external threads of the mating part. If manufacturing process permits, maximum hole size before threading should be maintained at the high end of the standard minor diameter limits.

30.3 Other considerations. When tapping relatively soft materials, especially with fine pitch threads, there is a tendency for the material to be squeezed down towards the root of the tap so that the minor diameter of the tapped hole may become smaller than the diameter of the drilled hole. It may be necessary to try a different size drill or different style tap to assure a satisfactory thread.

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	Threads	Desig-	Clas	ses 18 and 2 internal		ieter,		Tap dri	lls and pe	rcent of thre	ead and	
Thread size	per inch	nation	Minimum	Percent 1/ of thread	Maximum	Percent 1/ of thread	Drill	size	Percent of thread	Probable oversize, mean	Probable hole size	Percent of thread
in .060	80	UNF	in 0.0465	83.1	in 0.0514	53.0	(*56 <sup>in</sup>	in 0.0465 .0469	83 81	in 0.0015 .0015	in 0.0480 .0484	74 71
.073 .073	64 72	UNC UNF	.0561 .0580	83.3 83.1	.0623 .0635	52.7 52.7	● 54   ● 53   ● 53   √6	.0550 .0595 .0595 .0623	89 67 75 58	.0015 .0015 .0015 .0015	.0565 .0610 .0610 .0640	81 59 67 50
.086 .086	56 64	UNC UNF	.0667 .0691	83.2 83.3	.0737 .0753	53.0 52.7	# 51 # 50 # 49 # 50 # 49	.0670 .0700 .0730 .0700 .0730	82 69 56 79 64	.0017 .0017 .0017 .0017	.0687 .0717 .0747 .0717 .0717 .0747	75 62 49 70 56
. 099	48	טאט	.0764	83.5	.0845	53.6	#48 44 #47 #46 #45 #46	.0760 .0781 .0785 .0810 .0820 .0810	85 77 76 67	.0017 .0019 .0019 .0019 .0019 .0019 .0019	.0737 .0200 .0200 .0204 .0329 .0339 .0339 .0339 .0339	56 56 56
.099	56	UNF	.0797	83.2	.0865	53.9	#45 #44 (#44	.0820 .0860 .0860	63 78 73 56 80	.0019 .0019 .0019	.0379	65 48 74
.112 .112	40 48	UNC UNF	.0849 .0894	83.4 83.5	. 0939 . 0968	55.7 56.2	#43 #42 #43 #43 #42 #42 #41	.0890 .0935 .0938 .0890 .0935 .0938 .0960	80 71 56 85 68 67 59	.0020 .0020 .0020 .0020 .0020 .0020 .0020 .0020	.0910 .0955 .0958 .0910 .0955 .0958	65 51 50 78 61 60
.125	40	UNC UNF	.0979	83.4 - 83.3	. 1062	57.9 57.9	(#40 #39 #38` #37 #38 #37	.0980 .0995 .1015 .1040 .1015 .1040	83 79 72 65 80 71	.0023 .0023 .0023 .0023 .0023 .0023	.0380 .1003 .1018 .1038 .1063 .1038 .1038	52 76 71 65 58 72 63 55
. 138 . 138	32 40	UNC UNF	.104	83.8 83.1	.114	59.1 58.5	(#36 (#37 #36 !4 #35 #34 #33 (#34 #33 #32	.1065 .1040 .1065 .1094 .1100 .1110 .1130 .1110 .1130 .1160	63 84 78 70 69 67 62 83 77 68	.0023 .0023 .0023 .0023 .0026 .0026 .0026 .0026 .0026 .0026	.1088 .1088 .1088 .1120 .1126 .1126 .1136 .1136 .1156 .1156	55 78 72 64 63 60 55 75 69 60
. 164 . 164	32 36	UNC UNF	. 130 . 134	83.8 83.1	. 139 . 142	61.6 61.0	#29 [#29 #28 %	.1360 .1360 .1405 .1406	69 78 65 65	.6029 .0029 .0029 .0029	.1389 .1389 .1434 .1435	62 70 57 57
.190	24	UNC	. 145	83.1	. 15 <del>6</del>	62.8	( # 27 # 26 # 25 # 24 # 23	.1440 .1470 .1495 .1520 .1540	85 79 75 70 66	.0032 .0032 .0032 .0032 .0032	.1472 .1502 .1527 .1552 .1572	79 74 69 64 61 75
.190	32	UNF	.156	83.8	- 164	64.0	*6 # 22 # 21 # 20	.1562 .1570 .1590 .1610	83 81 76 71	.0032 .0032 .0032 .0032 .0032	.1594 .1603 .1622 .1642	75 73 68 64
.216	24	UNC	.171	83.1	. 181	64.7	11.6 17 16 15 19	.1719 .1730 .1770 .1800	82 79 72 67	.0035 .0035 .0035 .0035 .0035 .0035	. 1754 . 1765 . 1805 . 1835	75 73 66 60
.216	28	UNF	. 177	84.1	. 186	64.7	#16 #15 #14 #13 #14	.1770 .1800 .1820 .1850 .1850	84 78 73 67 84	.0035 .0035 .0035 .0035	.1805 .1835 .1855 .1885 .1885 .1855	75 73 60 77 70 66 59 75 68 62 58
.216	32	UNEF	. 182	83.8	.190	64.0	#13 #12	.1850 .1875 .1890	84 76 70 67	.0035 .0035 .0035	.1885 .1910 .1925	68 62 58

TABLE II.A.1 — Tap drill sizes, Unified screw threads, classes 1B and 2B
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See footnotes at end of table.

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			Cia	ises 18 and 28 internal		eter,		Tap dri	ils and perc	ent of threa	. I	
Thread size	Threads per inch	Desig- nation	Minimum	Percent 1/ of thread	Maximum	Percent 1/ of thread	Drill	size	Percent <sup>1</sup> of thread	Probable oversize, mean	Probable hole size	Percent <u>1</u> cf thread
in			in		in		(#9	in .1960	83	in .0038 .0038	in .1998	77
.250	20	UNC	.196	83.1	.207	66.2	#8 #7 <sup>13</sup> /4 #6 #5	.1990 .2010 .2031 .2040 .2055	83 79 75 72 71 69	.0038 .0038 .0038 .0038 .0038	.2028 .2048 .2069 .2078 .2093	77 73 70 65 63 72 59 63 72 63 70
. 250	28	UNF	211	84.1	.220	64.7	(#3	.2130	69 30 67	.0038	.2168 .2226	72 59
.250	32	UNEF	.216	83.8	.224	64.0 66.5	1/10 1/10 #2	.2188 .2210 .2210	77 71 80	.0038 .0038 .0038	.2228 .2248 .2248	62 70
. 250	36	UNS	.220	83.1	.226		#2 /F	.2210	77	.0038	.2608	
.3125	18	UNC	.252	83.8	. 265	65.8	GF	.2610	71	.0041 .0038	.2651 .2608	72 66 80 73 85
.3125	20	UN	.258	83.9	.270	65.4	G H	.2610 .2660	85 79 72	.0041 .0041	.2651 .2701	73 85
.3125	24	UNF	.267	84.1	.277	65.6	H I J	.2660 .2720 .2770 .2770	86 75 66 77	.0041 .0041 .0041 .0041	.2701 ,2761 ,2811 ,2811	78 67 58 68
.3125	28	UN	.274	83.0	.282	65.7	K %	.2810 .2812	68 67	.0042 .0042	.2852 ,2854	58 68 59 58
.3125	32	UNEF	.279	82.5	.288	65.3	(K % 7.25 mm	.2810	78 77	.0042	.2852 .2854	67 67 63
.3125	36	UNS	. 282	84.5	.289	65.1		.2854	75	.0042	.2896 .3169	
.375	16	UNC	.307	83.8	.321	66.5	O P	.3160	73 80 66 79	.0044	.3204 .3274	72 67 73
.375	20	UN	.321	83.1	.332	66.2	008	.3320	66	.0044	.3364 .3364	59 71
.375	24	UNF	.330	83.1	.340	64.7	R	.3390	1 67	.0044	.8434 .3434	58 68
.375	28	UN	.336	84.1	.345	64.7	111/16	.3438	78 67 77 67	.0045	.3483	58 66
.375 .375	32 36	UNEF UNS	.341	83.8 83.1	.349	64.0 63.7	8 8 8	.3480	87 75	.0045	.3525	73 59 71 58 68 58 68 55 66 55 62
.4375	14	UNC	.360	83.5	.376	66.3		.3580	86	.0046	.3626	81 79
.4375	16	UN	.370	83.1	.384	65.9		.3594 .3750 .3770	88 84 77 75 79 72 72	.0048	.3796	81 79 71 69 72 65 62
.4375	20	UNF	.383	83.9	.395	65.4	liw -	.3860	79	.0046	.3906	72
.4375	28	UNEF	.399	83.0	.407	65.7	13.64 Y	.3906	72	.0046	. 4086	62
.4375	32	UN	.404	825	.411	65.3	{Y 13/15	.4040	83 77	.0046	.4086	71 66
.500	12	UNS	.410	83.1	.428	66.5	(Z 1754 2754	.4130	80 72	.0047	.4177	76 68 73 71 65 57
.500	13 16	UNC	.417 .432	83.1 83.8	.434 .446	66.0 66.5	27,64	.4219	78	.0047	.4268	73
.500 .500 .500	1 20	UNE	.446	83.1 84.1	.457 .470	66.0 66.5 68.2 64.7	1/4 19/4 19/4 19/4	.4531	72 78 77 72 67	.0047	.4578 .4736	85 57
.500	28 32	UN	.466	83.8	.474	84.0	1	.4688	77	.0048	.4736	65
.5625	12	UNC	.472	83.6	.490	67.0	(15/m al/4 (15) (0.5062	.4688 .4844 .5000	87 72 77	.0048 .0048 .0048	.4736 .4892 .5048	82 68 71
.5625	16	UN	495	83.1	.509	65.9	0.5062	1 5082	69	1 0049	E110	63
.5625	18	UNF	.502	83.8	.515	65.8 65.4	0.5062 <sup>83</sup> 44	.5000 .5082 .5156	78	.0048	.5110	80 71 65
.5625	20	UN UNEF	.508	83.9 84.1	.520	65.6	$\begin{cases} 23 & 4 \\ 0.5203 \end{cases}$	.5156	87	.0048	.5204	65 78 69
.5625	28	UN	.524	83.0	.532	85.7	17/2 0.5283	.5203 .5312 .5263	78 67 78	.0049	.5361	57 67
. 5625	32	UN	.529	82.5	. 536	65.3	17/2	.5312	77			65
.625	11 12	UNC	.527	83.0 83.1	.546	66.9 66.5	17/13	.5312	79 72	.0049	.5361 .5518	75 68 71
.625	16	UN	.557	83.8	.571	66.5	0.5687	.5625 .5687 .5625	77	.0049	.5674	63
.625	18	UNF	. 565	83.1	.578	65.1	0.5687	.5687	87 78 72 87 78	.0049	.5674	63 80 71 65 78 69 57
.625	20	UN	.571	83.1	.582	66.2	1 17.44	.5781	72 87	.0049	.5830	85 78
.625 .625	24	UNEF	.580	83.1	.590	64.7	(0.5828	.5828	67	.0049	.5987	69 57
. 625	28 32	UN	.586 .591	84.1 83.8	.599	64.0	19	.5938	77	.0049		65

TABLE II.A.1 — Tap drill sizes, Unified screw threads, classes 1B and 2B — Continued

See footnotes at end of table.

	Throado		Clas	internal		ter,	Tap drills and porcent of thread					
Thread alzo	per inch	Desig- nation	Minimum	Percent 1/ of thread	Maximum	Percent of thread	Drill	stre	J/ Percent of throad	Probabie ovoraize, mean	Probable hole size	Percent of thread
in			ín	1	in		in	in		in	lin	1
.6875	12	UN	.597	83.6	.615	67.0	124	.5938	87 72	.0049	.5987	82
.6875	16	UN UN	.620	83.1	.634 .645	65.9	16	.6250	1 77	0.000	.6300	71
.6875	24	UNEF	.633	84.1	.652	65.6	1.2	.6406	72 87	.0050	6456	65
.6875 .6875 .6875 .6875	20 24 28 32	UN UN	.649 .654	83.1 83.9 84.1 83.0 82.5	.657 .681	65.6 65.6 65.7 65.3	1049 1144 1144 1144 1146 1146	.6562	87 67 77	.0050 .0050 .0050 .0050 .0050	.6300 .6456 .6456 .6456 .6612 .6612	82 68 71 65 71 57 65
.750	10	UNC	.642	83.1	.663	67.0		.6405	84 72	.0050	6450	
	12	UN	.660		.678		1.4	.6562	72 87	1 00ro	.6612 .6612 .6769	80 68 82 68 71
.750		-		83.1		66.5	192	.6719	87 72	.0050	.6769	68
.750	20	UNF UNEF	.682 .696	83.8 83.1	.696 .707	66.5 66.2 64.7	14 102	.6875	77 72	.0050	.6925	71
.750 .750 .750	16 20 28 32	UN UN	.711 .716	83.1 84.1 83.8	.707 .720 .724	64.7 64.0	1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.	.7188	67 77	.0050 .0050 .0050 .0050 .0051 .0051 .0051	.7239	64 56 64
8125	12	UN	.722	81.6	.740	67.0		7344			.7395	67
.8125 .8125 .8125 .8125 .8125	16	UN	.745	83.1 83.9 83.0	.759	65.9	*	1 7600	72 77 72	.0051 .0052 .0052	.7552	1 71
.8125	20 28	UNEF UN	.758 .774	83.9	.770 .782	65.4 65.7	10.44 11.2	.7656	72 67	.0052	.7708	64 56 64
.8125	o <b>32</b>	ŬŇ	.779	82.5	.786	65.3	14 X X X X X X X X X X X X X X X X X X X	.7812	67 77	.0052 .0052	.7864	64
.875	.9 12	UNC UN	.755	83.1	.778 .803	67.2	14 14 14 14	.7656	76 87 72	.0052	.7708 .7864	72
.875	12	UN	.785	83.1	.800	66.5	1.2	.7812 .7969	72	.0052 .0052 .0052 .0052 .0052 .0052 .0052 .0053 .0054 .0055 .0055	.8021	72 82 67 79 73 62 70 64 55 63
.875	14	UNF	.798	\$3.0	.814	65.7	0.8024	.7969	84 78 67 77 72 67	.0052	.8021	79
.875	16	UN	.807	83.8	.821	66.5	122	.8125 .8125	67	.0052	.8177	62
.875 .875	20	UNEF UN	.821 .836	83.1	.832 .845	66.5 66.2 64.7	53.4	.8281 .8438	72	.0054	.8335	64
.875	28 32	ŬŇ	.841	83.8 83.1 84.1 83.8	.849	64.0	1444	.8438	67 77	.0055 .0055	.8493 .8493	55 63
.9375	12	UN	.847	83.6	.885	67.0		.8438	87	.0055	.8493 .6650	81
.9375	16	UN	.870	83.1	.884 .895	65.9	14	.8594 .8750	72	.0056	.8850	67
.9375	20 28 32	UNEF	.883 .899	83.1 83.9 83 C	.895 .907	65.4	51 <sub>64</sub>	.8906	72	.0059	.8985	63
.9375 .9375	32	UN UN	.904	J2.5	.911	65.7 65.3	HAR AN	.9062 .9062	87 72 77 67 77	.0055 .0056 .0057 .0059 .0080 .0080	.9122 .9122	81 67 70 63 55 62
1.000	8	UNC	.865	83.1	. 690	67.7	(13.4 26	.8594	87	.0059 .0059	.8653 .8809	83
1.000	12	UNF	.910	83.1	.928	66.5	(124	.8750 .9082	77 87	.0080	.9122	73
1.000	14	UNS	.923	83.0	.938	66.8	10.9274	.9219 .9219	87 72 84 78 77 72	.0060	.9279 .9279 .9335	67 78
	16	UN	.932	83.8	.946	66.5	10.9274	.9274 .9375	78	.0061 .0062	.9335	72
1.000 1.000 1.000	20	UNEF	.946	83.1	.957	66.2	43 K	.9531	72	.0083	.9437 .9594	63
1.000	20 28 32	UN UN	.961 .966	847.1 83.8	.970 .974	64.7 64.0	474 174 174 174	.9688 .9688	67 77	.0065	.9753 .9753	83 73 81 67 78 72 69 83 53 61
1.0825	8	UN	.927	83.4	.952	68.0	0.9274	.9219 .9274	87 83	.0060 .0081	.9279 .9335	83 79
1.0625	12	UN	.972	83.6	.990	67.0	12.64	.9375 .9688	83 77 87 72	.0062	.9437	73 81
1.0625	16	UN	.995		1.009	65.9	11,2	.9844	72	.0087	.9911 1.0069 1.0069	66 68 77
1.0625	18	UNEF	1.002	83.8	1.015	65.8	i	1.0000	77 87	.0069	1.0069	77
1.0825	20 28	UN UN	1.008	83.1 83.8 83.9 83.0	1.020	65.4 65.7	1%	1.0156	72 67	.0070 .0071	1.0226	61 52
1.125	7	UNC	.970	83.5	.998	68.4		.8688	84	.0062	.9750	81
1.125	8	UN	.990	83.1	1.015	67.7	(****	.9844	76 77	.0087	.9911 1.0069	72 73 80 65
1.125	12	UNF	1.035	83.1	1.053		{i%	1.0312	87	.0071	1.0383	80
1.125	16	UN	1.057	83.8	1.071	66.5	11/4	1.0469	72 77	.0072	1.0541 1.0399	65 68
1.125	18	UNEF	1.065	83.1	1.078	65.1	11%	1.0325	87			•••••
1.125	20	UN UN	1.071	83.1	1.082	66.2 64.7	114	1.0781 1.0781	65 72			
1.125	28		1.088	84.1	1.095	1	116	1.0938	67	••••••		
1.1875	8 12	UN UN	1.052	83.4 83.6	1.077	68.0 67.0	1% 1%	1.0625	77 87			
1.1875	16	אט	1.120	83.1	1.134	65.9	144 144 (144 (144	1.1250	77 87	••••••		· · · · · · · · · · · ·
1.1875	18	UNEF	1.127	83.8	1.140	65.8	(i%	1.1406	65			
1.1875	20 28	UN UN	1.133	83.9 83.0	1.145 1.157	65.4 65.7	1%	1.1406	72 67			
1.250 1.250	7	UNC	1.095	83.5	1.123	1		1.0938	84			
I	8	UN	1.115	83.1	1.140	67.7	1% 1% (1%	1.1250 1.1562	77 87			
1.250	12	UNF	1.160	83.1	1.178		11-16	1.1719	72			
1.250	16	UN	1.182	83.8	1.198	66.5	126	1.1875	77 87			• • • • • • • • • • • • • • • • • • •
1.250	18	UNEF	1.190	83.1	1.203	65.1	(1½) (1½) (1)	1.2031	65			
1.250	20 28	UN UN	1.198	83.1 84.1	1.207	66.2 64.7	11/2	1.2031	72 67			
		[	1			••••			•			

TABLE II.A.1 - Tap drill sizes, Unified screw threads, classes 1B and 2B - Continued

See footnotes at end of table.

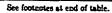
	Threads		Cla	sses 18 and 2 internal		neter,	Tap drills and percent of thread						
'hread size	per inch	Desig - nation	Minimum	Percent of thread	Maximum	1/ Percent of thread	Dril	l size	_]/ Percent of thread	Probable oversize, mean	Probable hole size	Percent of thread	
in		1 .	in	<u> </u>	in		in	in		in	in		
1.3125	· 8	UN	1.177	83.4	1.202	68.0	1 <sup>11</sup> 64 1 <sup>3</sup> /16	1.1719 1.1875 1.2188	87 77				
1.3125	12	UN	1.222	83.6	1.240	67.0	11/32	1.2188	87 72				
1.3125	16	UN	1.245	83.1	1.259	65.9	114	1.2500	77				
1.3125	18	UNEF	1.252	83.8	1.265	65.8	11/4 (11/4 (11/4)	1.2500	87 65				
1.3125	20	UN UN	1.258	83.9	1.270	65.4	111764	1.2656	72				
1.3125	28	UN	1.274	83.0	1.282	65.7	1%2	1.2812	67				
1.375	6	UNC	1.195	83.1	1.225	69.3	$ \begin{bmatrix} 1^{3} \\ 1^{15} \\ 64 \\ 1^{15} \\ 64 \end{bmatrix} $	1.1875 1.2031 1.2188	87 79 72				
1.375	8	UN	1.240	83.1	1.265	67.7	115.64	1.2344 1.2500 1.2812	87 77 87 72 77 87				
1.375	12	UNF	1.285	83.1	1.303	66.5	1942 11942	1.2812	87				
1.375	16	UN	1.307	83.8	1.321	66.5	15/16	1.2969 1.3125 1.3125	72				
1.375	18	UNEF	1.315	83.1	1.328	65.1	15 16 1 21 64	1.3125	87 65				
1.375	20	UN	1.321	83.1	1.332	66.2	111/4	1.3281 1.3281 1.3438	72				
1.375	28	ŪN	1.336	84.1	1.345	. 64.7	11/2		67				
1.4375	6	UN	1.257	83.4	1.288	69.1	11/14 19/12	1.2656 1.2812 1.2969 1.3125	79 72				
1.4375	8	UN	1.302	83.4	1.327	68.0	11.64	1.2969	87 77				
			1		1		111/2	1.3438	87				
1.4375	12	UN UN	1.347	83.6 83.1	1.365	67.0	1 23/4	1.3438 1.3594 1.3750 1.3750 1.3750	87 72 77				
$\begin{array}{r}1.4375\\1.4375\\1.4375\\1.4375\end{array}$	16 18	UNEF	1.370 1.377	83.8	1.390	65.8	1 <sup>3</sup> /8 1 <sup>3</sup> /8	1.3750	87 72				
$1.4375 \\ 1.4375$	20 28	UN UN	1.383	83.9 83.0	1.395	65.9 65.8 65.4 65.7	125,64	1.3906	67				
1 500		UNC	1 220	97.1	1.350	69.3	115/16	1.3125	87	]			
1.500	6	UNC	1.320	83.1			121 64 123 64	1.3281 1.3594	87 79 87				
1.500	8	UN	1.365	83.1	1.390	67.7	113%	1.3750	77				
1.500	12	UNF	1.410	83.1	1.428	66.5	113/2	1.4062	77 87 72 77 87 87 72				
1.500	16	UN	1.432	83.8	1.446	66.5	17/16	1.4375	87				
1.500 1.500 1.500	18 20	UNEF UN	1.440	83.1 83.1	1.452	66.5 66.2 64.7	1 29 54 1 15 52	1.4531	72				
1.500	28	ÚN	1.461	84.1	1.470	64.7		1.4688	67				
1.5625	6	UN	1.382	83.4	1.413	69.1	125 64 113 64	1.3906	79 72				
1.5625	8	UN	1.427	83.4	1.452	68.0	12764	1.4219	87 77 87 72 77				
1.5625	12	UN	1.472	83.6	1.490	67.0	115%	1.4688	87				
1.5625	16	UN	1.495	83.1	1.509	65.9	111/2 11/2 /11/2	1.5000	77				
1.5625	18	UNEF	1.502	83.8	1.515	65.8	11.2 11.2 11.2 11.2 1	1.5000	87 65				
1.5625	20	UN	1.508	83.9	1.520	65.4	133%4	1.5156	72				
1.625	-6	UN	1.445	83.1	1.475	69.3	129 64 115 22	1.4531 1.4688 1.4844 1.5000 1.5312	79 72	• • • • • • • • • • • •			
1.625	8	UN	1.490	83.1	1.515	67.7	1131/04	1.4844	87 77				
	1.1.1			1			11/2	1.5312	87 72				
1.625	12	UN	1.535	83.1	1.553	66.5	1357	1.5469	72 77				
1.625	16	UN	1.557	83.8 83.1	1.571 1.578	66.5 65.1	1 % 18 { 1 % 18 { 1 <sup>37</sup> 64	1.5625	87				
1.625 1.625	18 20	UNEF UN	1.571	83.1	1.578	66.2	13764	1.5625 1.5781 1.5781	65 72				
							(11/2 11/2 11/2		87 79				
1.6875	6	UN	1.507	83.4	1.538	69.1	11%	1.5000 1.5156 1.5312	72				
1.6875	8	UN	1.552	83.4	1.577	68.0	117/2 19/16 (119/13	1.5625 1.5938	77				
1.6875	12	UN	1.597	83.6	1.615	67.0	1 204	1.6094	87 72 77				
1.6875	16	UN	1.620	83.1	1.634	65.9	1129 15/8 115/8	1.6250	87				
1.6875	18	UNEF	1.627	83.8	1.640	65.8	114.64	1.6406	65				
1.6875	20	UN	1.633	83.9	1.645	65.4	144	1.6406	72				
1.750	5	UNC	1.534	83.1	1.568	70.1	{1 <sup>17</sup> / <sub>22</sub> 1 <sup>35</sup> / <sub>64</sub> 1 <sup>9</sup> / <sub>6</sub> 1 <sup>37</sup> / <sub>64</sub> 1 <sup>19</sup> / <sub>75</sub>	1.5312 1.5469 1.5625 1.5781 1.5938 1.6094 1.6250 1.6406	84 78 97				
1.750	6	UN	1.570	83.1	1.600	69.3	1 37	1.5625	87 79				
							1192	1.5938	72				
1.750	8	UN	1.615	83.1	1.640	67.7	1 39 64 1 5 % 1 4 %	1.6250	87 77 67				
1.750	12	UN	1.660	83.1	1.678	66.5	1(12)/4	1 1.0002	87				
1.750	12	UN	1.682	83.8	1.696	66.5	14364	1.6719	87 72 77 77 72				
1.750	20	ŬŇ	1.696	83.1	1.707	66.2	145.64	1.7031	72		.	•   • • • • • • • •	

TABLE II.A.1 - Tap drill sizes, Unified screw threads, classes 1B and 2B - Continued

See footnotes at end of table.

	Threads		Cla	sses 18 and 2 internal		noter,	Tap drill and percent of thread							
Thread size	por inch	Desig – nation	Minlmum	Percent <sup>1</sup> of thread	Maximum	Parcent 1/ of thread	Drill	sizo	Percent of thread	Probable oversize, mean	Probable hole size	Percent		
in	1	1	in		in		ín	in		1	1	1		
1.8125	6	UN	1.632	83.4	1.663	69.1	1.5%	1.6250	87 79					
1.0125	°	UN	1.052	00.4	1.005	09.1	122	1.6582	72					
1.8125	8	UN	1.677	83.4	1.702	68.0	197 197 197	1.6719	87 77 87 72					
		7157	1 700	83.6	1 740		112/2	1.7188	87	•••••				
1.8125	12	UN	1.722		1.740	67.0	ligz	1.7344	72					
1.8125 1.8125	16 20	UN UN	1.745 1.758	83.1 83.9	1.759 1.770	65.9 65.4	1192 192 194 194	1.7500 1.7656	77 72					
1.875	6	UN	1.695	83.1	1.725	69.3	[194	1.7031	79					
1.875	8	UN	1.740	83.1	1.765	67.7	(144) 194 194	1.7188	72 77		<b> </b>			
1.875	12	UN	1.785	83.1	1.803	66.5	111-26	1.7812	87					
1.875	16	UN	1.807	83.8	1.821	66.5	11%	1.7969	72 77					
1.875	20	ŬŇ	1.821	83.1	1.832	66.2	iug	1.8281	72					
							11%	1.7656	79		ľ			
1.9375	6	UN	1.757	83.4	1.788	69.1	1112/2	1.7812	72					
1.9375	8	UN	1.802	83.4	1.827	68.0	(19)2 (19)2	1.7969	87 77		·····			
		-	1				ing a	1.8438	87					
1.9375	12	UN	1.847	83.6	1.865	67.0	11.2	1.8594	87 72 77					
1.9375	16 20	UN UN	1.870	83.1 83.9	1.884 1.895	65.9 65.4	114 114 126 114	1.8750	77		[- <i>-</i>	<i>-</i>		
		-												
2.000	4.5	UNC	1.759	83.5	1.795	71.0	1124 (1644 (1776	1.7812 1.8281	76 79					
2.000	6	UN	1.820	83.1	1.850	69.3	1172	1 1 2472	72					
2.000	8	UN	1.865	83.1	1.890	67.7	196	1.8750	79 72 77 87 72 77 72 72					
2.000	12	UN	1.910	83.1	1.928	66.5	(11%) (11%) 11%) 11%)	1.9062	72					
2.000	16	ŲŊ	1.932	83.8	1.946	66.5 66.2	11%	1.9375	77					
2.000	20	UN	1.946	83.1	1.957	66.2	1.4	1.9531	72	******		•••••		
2.0625	16	UNS	1.995	83.1	2.009	65.9	2	2.0000	77					
2.125	6	UN	1.945	83.1	1.975	69.3	(1•%) 1•%	1.9531	79					
2.125	8	UN	1,990	83.1	2.015		2	1.9688 2.0000	72 77					
2.125	12	ÜN	2.035	83.1	2.053	66.5	21/6	2.0312	87					
2.125 2.125	16 20	ÛN UN	2.057 2.071	83.8 83.1	2.071 2.082	67.7 66.5 66.5 66.3	21/6 21/6 21/6	2.0625	77 96					
		- ·												
2.1875	16	UNS	2.120	83.1	2.134	65.9	256 J2	2.1250 2.0000	77 87					
2.250	4.5	UNC	* 2.090	83.5	2.045	71.0	1212	2.0312	78					
2.250 2.250	6 8	UN UN UN	2.070 2.115	83.1	2.100 2.140	69.3	21/4	2.0625 2.1250	87 77					
2.250	12	ŬŇ	2.160	83.1 83.1	2.178	66.5	21/0	2.1562	87 77					
2.250 2.250	16 20	ŬN UN	2.182 2.196	83.8 83.1	2.196 2.207	69.3 67.7 66.5 66.5 66.2	214	2.1875 2.1875	77 96					
2.3125	16	UNS	2.100	83.1 83.1	2.207	65.9	234	2.2500	77					
2.375 2.375	6 8	UN UN	2.195 2.240	83.1	2.226 2.285	68.8 67.7	234 214 58 mm	2.1875 2.2500	87 77 85 77			••••		
2.375	12	UN	2.285 2.307	83.1	2.303	66.5	58 mm	2.2500 2.2835 2.3125	85					
2.375	16 20	UN UN	2.307 2.321	83.1 83.1 83.1 83.8 83.8 83.1	$2.321 \\ 2.332$	66.5 66.2	21/4	$2.3125 \\ 2.3125$	77 96		•••••			
2.4375	16	UNS	2.370	83.1 83.1	2.384	65.9	2%	2.3750	77		•••••	•••••		
							-							
2.500	4	UNC	2.229	83.4	2.267	71.7	21/4 21/4	2.2188 2.2500	87 77					
2.500	6	UN	2.320	83.1	2.350	69.3	24	2.2500 2.3125	87					
2.500	8 12	UN UN	2.365 2.410	83.1 83.1	2.390 2.428	67.7 66.5	24 29 21 21	2.3750 2.4062	77 87					
2.500	16	UN	2.432	83.8	2.446	66.5	21/4 21/4	2.4375	77					
2.500	20	ÚN	2.446	83.1	2.457	66.2		2.4375	96					
2.625	4	UN	2.354	83.4	2.392	71.7	(211,6	2.3438	87					
2.625	6	UN	2.445	83.1	2.475	69.3	122224	2.3750 2.4375	77 87	•••••	•••••			
2.625	8	UN	2.490	83.1	2.515	67.7	23	2.5000	77					
2.625	12 16	UN UN	2.535 2.557	83.1 83.8	2.553 2.571	66.5 66.5	21/4	2.5312	87 77			•••••		
2.625	20	บัก	2.571	83.1	2.582	66.2	2% 2%	2.5625 2.5625	77 96					
2.750	4	UNC	2.479											
2.750	6	UNUN	2.570	83.4 83.1	2.517 2.600	71.7 69.3	214 256 236 236 246 246 246 246 246 246	2.5000 2.5625	77 87					
2.750 2.750	8 12	UN	2.615	83.1	2.640	67.7	2%	2.6250	87 77 87					
		UN	2.660	83.1 83.8 83.1	2.678	66.5	21/6	2.6562	87					
2.750	16	UN	2.682	<b>XX X 1</b>	2.696	66.5	2012	2.6875	77					

TABLE II.A.1 - Top drill sizes, Unified screw threads, classes 18 and 28 - Continued





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I		Desig— nation	Classes 1B and 2B minor diameter, internal threads					Tap drill and percent of thread						
fhread size	Threads per inch		Minimum	Percent of Thread	Maximum	Percent <sup>1/</sup> of Thread		Drill size	Percent of Thread	Probable oversize, mean	Probable hole size	Percent of Thread		
in 2.875 2.875 2.875 2.875 2.875 2.875 2.875 2.875	4 6 8 12 16 20	UN UN UN UN UN UN UNC	in 2.604 2.695 2.740 2.785 2.807 2.821 2.729	83.4 83.1 83.1 83.1 83.8 83.1 83.4	in 2.642 2.725 2.765 2.803 2.821 2.832 2.767	71.7 69.3 67.7 66.5 66.5 66.2 71.7	in 25/8 211/15 23/4 213/15 213/15 213/15 213/15 23/	in 2,6250 2,6875 2,7500 2,7812 2,8125 2,8125 2,7500	77 87 77 87 87 77 96					
3.000 3.000 3.000 3.000 3.000 3.000	4 6 8 12 16 20	UN UN UN UN UN	2.729 2.820 2.865 2.910 2.932 2.946	83.4 83.1 83.1 83.1 83.8 83.8 83.1	2.907 2.850 2.928 2.928 2.946 2.957	69.3 67.7 66.5 66.5 66.2	234 213,66 27,8 74 mm 213,66 213,66 213,16	2.9305 2.8125 2.8750 2.9134 2.9375 2.9375	87 77 80 77 96					
3.250 3.500 3.750	4	UNC UNC UNC	2.979 3.229 3.479	83.4 83.4 83.4	3.017 3.267 3.517	71.7 71.7 71.7	3 314 315	3.0000 3.2500 3.5000	77 77 77					

TABLE II.A.1 - To	ıp drill sizes	Unified screw threads, classes	s 1B and 2B - Continued
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1/ 100% of thread = 0.75H (see 20.2.3).

		ľ	ſ			265, 011110								
	Threads		Class 3B	minor diamete	r, internal thr	reads	Tap drill and percent of thread							
Thread size	Threads per inch	Desig - nation	Minimum	1/ Percent of Thread	Maximum	니. Percent of Thread	Dr	ill size	) Percent of Thread	Probable oversize, mean	Probable hole sìze	Percent of Thread		
in .060	80	UNF	in 0.0465	83.1	in 0.0514	52.9	in {#56 364	in 0.0465 .0469	83 81	in 0.0015 .0015	in 0.0480 .0484	74 71		
.073	64	UNC	.0561	83.3	.0623	52.7	{ #54   #53	.0550 .0595	89 67	.0015 .0015	.0565 .0610	81 59		
.073	72	UNF	.0580	83.1	.0635	52.7	# 53   1/4	.0595 .0625	75 58	.0015	.0610	67 50		
.086	56	UNC	.0667	83.2	.0737	53.0	(#51 {#50  #49	.0670 .0700 .0730	82 69 56	.0017 .0017 .0017	.0687 .0717 .0747	75 62 49		
.086	64	UNF	.0691	83.3	.0753	52.7	(#50 (#49	.0700	79 64	.0017 .0017	.0717 .0747	70 56		
. 099	48 56	UNC	.0764	83.5	.0845	53.6	{#48 <sup>5</sup> ∕4 {#47 #46 #45 {#48 {#45	.0760 .0781 .0785 .0810 .0820 .0810 .0820	85 77 76 67 63 78 73	.0019 .0019 .0019 .0019 .0019 .0019 .0019 .0019	.0779 .0800 .0804 .0829 .0839 .0839 .0829 .0839	78 70 69 60 56 69 65 48		
.112	40	UNC	.0849	83.4	.0939	55.7	#44 #43 #42 % #43	.0860 .0860 .0890 .0935 .0938	56 80 71 57 56 85	.0019 .0020 .0020 .0020 .0020 .0020	.0879 .0879 .0910 .0955 .0958 .0958	48 74 65 51 50 78 81 60		
.112	48	UNF	.0894	83.5	.0968	56.2	#42 *42 *6 #41	.0890 .0935 .0938 .0960	68 67 59	.0020 .0020 .0020	.0955 .0958 .0980	61 60 52		
.125	40	UNC	.0979	83.4	.1062	57.9	(#40 #39 #38 #37 #38	.0980 .0995 .1015 .1040 .1015	83 79 72 65 80 71	.0023 .0023 .0023 .0023 .0023 .0023	.1003 .1018 .1038 .1063 .1038	7 <del>6</del> 71 65 58 72 63 55		
. 125	44	UNF	.1004	- 83.3	. 1079	57.9	#37 #36	.1013	71 63	.0023	.1063	63 55		
.138	32	UNC	.1040	83.8	.1140	59.1	(#37 #36 %4 #35 #34 #33	.1040 .1065 .1094 .1100 .1110 .1130	84 78 70 69 67 52	.0023 .0023 .0026 .0026 .0026 .0026	.1063 .1088 .1120 .1126 .1136 .1156	78 72 64 63 60 55 75 69 60		
. 138	40	UNF	.1110	83.1	.1186	59.7	#34 #33 #32	.1110 .1130 .1160	83 77 68	.0026 .0026 .0026	.1136 .1156 .1186	75 69 60		

TABLE II.A.2 - Tap drill sizes, Unified screw threads, class 3B

See footnotes at end of table.

in .184 .184 .190 .190 .190 .216 .216 .216 .216 .216 .216 .216 .216 .216 .216 .216 .250 .250 .3125 .3125 .3125 .3125 .3125 .3125 .3125	Incode         32         36         24         32         24         32         24         32         24         32         24         32         24         32         24         32         28         32         18	UNC UNF UNC UNF UNC UNF UNC UNF UNC UNF UNC	Minlmum in .1300 .1340 .1450 .1450 .1560 .1710 .1770 .1820 .1960 .2110 .2160	Percent 1/ of Thread 83.8 83.1 83.8 83.1 84.1 83.8 83.1 84.1 83.8 83.1	Maximum in .1389 .1416 .1555 .1641 .1807 .1807 .1805 .2067 .2190 .2229	Percent <sup>1</sup> of Thread 61.8 62.1 63.7 63.6 63.8 65.3 65.3 65.3 65.3 65.3 65.3 65.3	1000         1000         1000         1000         1000         1000         1000         1000         1000         1000         1000         1100         1100         1100         1100         1110 <t< th=""><th>t size in 1360 1360 1405 1406 1406 1406 1406 1406 1470 1495 1520 1540 1560 1560 1570 1570 1600 1800 1820 1820 1820 1850 1820 1855 1820 1855 1820 1855 1820 1855 1820 1855 1820 1855 1820 1855 1820 1855 1820 1855 1820 1855 1820 1857 1820 1850 1960</th><th>Percent of Thread 69 78 65 65 65 65 65 65 65 79 75 70 66 83 81 81 76 71 82 79 72 67 84 73 67 84 70 67 84 85 67 77 75 70 67 84 85 70 85 70 75 70 67 85 70 77 77 77 77 77 77 77 77 77 77 77 77</th><th>Probable oversize, mean 0029 0029 0029 0029 0029 0032 0032 0032</th><th>Probable bole size 1389 1389 1434 1435 1434 1435 1437 1502 1572 1572 1572 1572 1572 1572 1572 157</th><th>Percent of Thread 62 70 57 57 57 79 69 64 61 75 73 68 68 64 64 75 73 66 68 66 77 70 70 66 55 68 62 62 53 77 73 70 70 70 70 70 70 70 70 70 70 70 70 70</th></t<>	t size in 1360 1360 1405 1406 1406 1406 1406 1406 1470 1495 1520 1540 1560 1560 1570 1570 1600 1800 1820 1820 1820 1850 1820 1855 1820 1855 1820 1855 1820 1855 1820 1855 1820 1855 1820 1855 1820 1855 1820 1855 1820 1855 1820 1857 1820 1850 1960	Percent of Thread 69 78 65 65 65 65 65 65 65 79 75 70 66 83 81 81 76 71 82 79 72 67 84 73 67 84 70 67 84 85 67 77 75 70 67 84 85 70 85 70 75 70 67 85 70 77 77 77 77 77 77 77 77 77 77 77 77	Probable oversize, mean 0029 0029 0029 0029 0029 0032 0032 0032	Probable bole size 1389 1389 1434 1435 1434 1435 1437 1502 1572 1572 1572 1572 1572 1572 1572 157	Percent of Thread 62 70 57 57 57 79 69 64 61 75 73 68 68 64 64 75 73 66 68 66 77 70 70 66 55 68 62 62 53 77 73 70 70 70 70 70 70 70 70 70 70 70 70 70
. 164 . 164 . 190 . 190 . 190 . 216 . 216 . 216 . 216 . 216 . 216 . 250 . 250 . 3125 . 3125	36 24 32 24 28 32 20 28 32	UNF UNC UNF UNF UNEF UNC UNF UNEF	.1300 .1340 .1450 .1560 .1710 .1770 .1820 .1960 .2110 .2160	83.1 83.1 83.8 83.1 84.1 83.8 83.1 84.1	.1389 .1418 .1555 .1641 .1807 .1807 .1805 .2067 .2190	62.1 63.7 63.8 05.2 65.3 65.3 66.7 66.8	$\begin{array}{c} 229\\ 229\\ 228\\ 16\\ 228\\ 16\\ 226\\ 226\\ 226\\ 226\\ 223\\ 224\\ 223\\ 22\\ 221\\ 221\\ 220\\ 221\\ 220\\ 221\\ 220\\ 216\\ 216\\ 215\\ 216\\ 215\\ 216\\ 215\\ 216\\ 215\\ 216\\ 216\\ 215\\ 216\\ 216\\ 215\\ 216\\ 216\\ 216\\ 216\\ 216\\ 216\\ 216\\ 216$	1360 1360 1405 1406 1406 1470 1470 1470 1540 1550 1560 1560 1770 1600 1770 1800 1770 1800 1820 1850 1850 1855 1850 1990 2010 2010 2010 2010	85 79 750 86 81 70 84 81 70 70 70 70 84 87 81 84 87 81 67 67	.0029 .0029 .0032 .0032 .0032 .0032 .0032 .0032 .0032 .0032 .0032 .0032 .0032 .0032 .0035	. 1389 . 1389 . 1434 . 1435 . 1472 . 1502 . 1527 . 1552 . 1552 . 1552 . 1552 . 1652 . 1602 . 1602 . 1603 . 1605 . 1805 . 1805 . 1805 . 1855 . 1910 . 1925	57 79 64 61 75 73 68 64 75 73 68 64 75 73 68 60 77 70 66 59 75 68 862 53
. 190 . 190 . 216 . 3125 . 3155 . 31555 . 31555 . 31555555555555555555555555555555555555	24 32 24 28 32 20 28 32	UNC UNF UNC UNF UNC UNF UNF	. 1450 . 1560 . 1710 . 1770 . 1820 . 1960 . 2110 . 2160	83.1 83.8 83.1 84.1 83.8 83.1 84.1	. 1555 . 1641 . 1807 . 1857 . 1895 . 2067 . 2190	63.7 63.8 05.3 05.3 06.7 06.8	1%G         # 226         # 225         # 226         # 221         # 221         # 221         # 221         # 20         114         # 116         # 115         # 116         # 116         # 116         # 116         # 116         # 116         # 116         # 116         # 116         # 116         # 116         # 116         # 116         # 116         # 117         # 118	1403 1406 1440 1470 1495 1520 1562 1570 1562 1570 1610 1770 1800 1800 1800 1820 1850 1850 1850 1850 1850 1850 1850 185	85 79 750 86 81 70 84 81 70 70 70 70 84 87 81 84 87 81 67 67	.0029 .0032 .0032 .0032 .0032 .0032 .0032 .0032 .0032 .0032 .0035 .0032 .0035	.1435 .1472 .1502 .1527 .1522 .1572 .1572 .1572 .1602 .1602 .1602 .1602 .1602 .1603 .1805 .1805 .1805 .1805 .1805 .1855 .1855 .1855 .1855 .1855 .1910 .1925	57 79 64 61 75 73 68 64 75 73 68 64 75 73 68 60 77 70 66 59 75 68 862 53
. 190 . 216 . 216 . 216 . 216 . 218 . 250 . 250 . 250 . 3125 . 375	32 24 28 32 20 28 32	UNF UNC UNF UNC UNC UNF UNEF	.1560 .1710 .1770 .1820 .1960 .2110 .2160	83.8 83.1 84.1 83.8 83.1 84.1	. 1641 . 1807 . 1857 . 1895 . 2067 . 2190	63.8 (5.2 65.3 (5.3 (66.7 (66.8	$\begin{array}{c} $ 226 \\ $ 223 \\ $ 224 \\ $ 223 \\ $ 35 \\ $ 422 \\ $ 221 \\ $ $ 221 \\ $ $ $ 221 \\ $ $ $ $ $ $ $ $ $ $ $ $ $ $ $ $ $ $ $	1470 1495 1520 1562 1570 1562 1570 1610 1719 1770 1800 1870 1800 1870 1850 1850 1850 1850 1850 1850 1850 185	75 70 83 86 71 829 72 67 84 84 78 84 84 70 67	.0032 .0032 .0032 .0032 .0032 .0032 .0032 .0035	. 1502 1527 1552 1552 1552 1552 1552 1622 1622 1642 1754 1765 1805 1835 1835 1835 1835 1855 1855 1855 185	74 69 64 75 73 68 64 75 73 68 60 777 70 66 65 55 55 68 62 38
.216 .216 .216 .216 .250 .250 .3125 .3125 .3125 .3125 .3125 .3125 .3125	24 28 32 20 28 32	UNC UNF UNEF UNC UNF UNEF	.1710 .1770 .1820 .1960 .2110 .2160	83.1 84.1 83.8 83.1 84.1	. 1807 . 1857 . 1895 . 2067 . 2190	65.3 65.3 66.7 66.8	$\begin{array}{c} $ $ $ $ $ $ $ $ $ $ $ $ $ $ $ $ $ $ $$	1570 1590 1610 1719 1770 1800 1870 1800 1850 1850 1850 1850 1850 1850 185	76 71 82 79 72 67 84 87 87 87 87 87 87 87 87 87 87 67	.0032 .0032 .0035 .0035 .0035 .0035 .0035 .0035 .0035 .0035 .0035 .0035 .0035 .0035 .0035 .0035 .0035 .0035 .0035	. 1622 . 1642 . 1754 . 1765 . 1805 . 1805 . 1805 . 1855 . 1855 . 1855 . 1855 . 1855 . 1855 . 1855 . 1855 . 1855 . 1910 . 1925	75 66 60 77 70 66 59 75 68 62 62 38
.216 .216 .250 .250 .3125 .3125 .3125 .3125 .3125 .3125 .3125 .3125	28 32 20 28 32	UNF UNEF UNC UNF UNEF	.1770 .1820 .1960 .2110 .2160	84.1 83.8 83.1 84.1	. 1857 . 1895 . 2067 . 2190	65.3 65.3 66.7 66.8	#17 #16 #15 #15 #15 #14 #13 #14 #13 #14 #13  #14 #13  #14 #13  #12  #12  #9 #8 #8 #5 #5 #5 #5	. 1770 . 1800 . 1800 . 1800 . 1820 . 1850 . 1960 . 2031 . 2040 . 2040	67 84 78 73 67 84 76 70 67	.0035 .0035 .0035 .0035 .0035 .0035 .0035 .0035 .0035 .0033 .0033 .0038 .0038	.1805 .1835 .1805 .1835 .1855 .1855 .1855 .1855 .1855 .1855 .1910 .1925	
.216 .250 .250 .3125 .3125 .3125 .3125 .3125 .3125 .3125 .3125	32 20 28 32	UNEF UNC UNF UNEF	. 1820 . 1960 . 2110 . 2160	83.8 83.1 84.1	. 1895 . 2067 . 2190	6.5.3 66.7 66.8	#15 #14 #13 #14 #13 #14 #13 #14 #13 #14 #13 #14 #13 #14 #13 #14 #15 #14 #15 #14 #15 #14 #15 #14 #13 #14 #13 #14 #13 #14 #13 #14 #13 #14 #13 #14 #13 #14 #13 #14 #13 #14 #15 #14 #15 #14 #15 #14 #15 #14 #15 #14 #15 #14 #15 #14 #15 #14 #15 #14 #15 #14 #15 #15 #14 #15 #16 #15 #16 #15 #16 #15 #16 #15 #16 #15 #16 #15 #16 #15 #16 #15 #16 #15 #16 #15 #16 #15 #16 #15 #16 #15 #16 #15 #16 #15 #16 #15 #16 #16 #15 #16 #15 #16 #16 #16 #16 #17 #16 #16 #16 #16 #16 #16 #16 #16 #16 #16	. 1854) . 1875 . 1890 . 1960 . 2010 . 2031 . 2040 . 2055 . 2130		.0035 .0035 .0035 .0035 .0035 .0035 .0035 .0035 .0035 .0038 .0038	.1885 .1910 .1925	
.250 .250 .250 .3125 .3125 .3125 .3125 .3125 .3125 .3125 .3125	20 28 32	UNC UNF UNEF	. 1960 . 2110 . 2160	83.1 84.1	.2067 .2190	66.7 66.8	#13 *: #9 #8 #7 *: #6 #5 #3 *: *:	. 1854) . 1875 . 1890 . 1960 . 2010 . 2031 . 2040 . 2055 . 2130		.0035 .0035 .0035 .0038 .0038	.1885 .1910 .1925	
.250 .250 .3125 .3125 .3125 .3125 .3125 .3125 .3125 .3125	28 32	UNF UNEF	. 2110 . 2160	84.1	.2190	66.8	#8 #7 134 #0 #5 (#3 14	.1990 .2010 .2031 .2040 .2055 .2130	83 79 75 72 71 69 80 67	.0038 .0038 .0038 .0038 .0038 .0038 .0038 .0038	.1998 .2028 .2048 .2069 .2078 .2093 .2168 .2226	77 73 70 68 65 63 72 59
.250 .3125 .3125 .3125 .3125 .3125 .3125 .3125 .3125	32	UNEF	. 2160				1 #3 1/2	.2130	80 67	.0038	.2168 .2226	72 59
.3125 .3125 .3125 .3125 .3125 .3125 .3125				83.8	.2229	66.8	1.000	2100	77	0038		87
.3125 .3125 .3125 .3125 .3125 .3125	18	UNC			1		***2	.2188 .2210				
.3125 .3125 .3125 .3125			. 2520	83.8	.2630	68.6		.2570 .2610 .2570	77 71 85	.0038 .0041 .0038	.2608 .2651	72 66 80
.3125 .3125 .375	20	UN	. 2580	83.9	. 2680	68.5	G	.2610	77 71 85 79 72 88 75 75 77 78 77	.0041 .0041	.2651 .2701	72 66 80 73 65 78 67 68 67 67
.3125 .375	24	UNF	.2670	84.1	.2754	68.5	(H	.2660 .2720	88 75	.0041 .0041	.2701 .2761	78 67
	28 32	UN UNEF	.2740 .2790	83.0 82.5	.2807 .2847	68.5 68.5	K (***	.2770 .2810 .2812	78 78 77	.0041 .0042 .0042	.2608 .2651 .2608 .2651 .2701 .2701 .2761 .2811 .2852 .2854	67 67
.375 .375 .375 .375	16	UNC	.3070	83.8	.3182	70.0	(). (O	.3125 .3160	77 73	.0044 .0044	.3169 .3204 .3274	72 67 73 71
.375 .375	20 24	UN UNF	.3210 .3300	83.1 83.1	.3297 .3372	69.7 69.8	1 P	.3230 .3320	80 79	.0044	.3274 .3364	73 71
	20 24 28 32	UN UNEF	.3360 .3410	84.1 83.8	.3426 .3469	69.8 69.2	Q R <sup>11</sup> á	.3390 .3438	78 77	.0044 .0045	.3434 .3483	68 66
.4375	14	UNC	.3600	83.5	.3717	70.9	{T 136	.3580 .3594	86 84 77	.0046 .0046	.3626 .3640 .3736	81 79
. 4375	16	UN	.3700	83.1	.3800	70.8	V V	.3750 .3770 .3860	75	.0046 .0046	.35.6	71 69 72
.4375	20	UNF	.3830	83.9	.3916	70.7	( <sup>22,</sup> M	.3860 .3906	79 72	.0046 .0046	.3906 .3952	72 65
	28 32	UNEF UN	.3990 .4040	83.0 82.5	.4051 .4094	69.8 69.2	Y {Y (1) <sub>12</sub>	.4040 .4040 .4062	72 83 77	.0046 .0046 .004 <u>6</u>	.4086 .4086 .4108	62 71 66
	12	UNS	. 4100	83.1	. 4223	71.8	2	.4130 .4219	80 72	.0047	.4177	76 68 73
.500	13   16	UNC UN	.4170	83.1 83.8	.4284 .4419	71.7 71.6	1.00	.4219 .4375	78	.0047	.4266	71
.500 .500 .500	16 20 28 32	UNF UNEF UN	.4460 .4610 .4660	83.1 84.1 83.8	.4537 .4676 .4719	71.3 69.8 69.2	11.8 mm	.4531 .4646 .4688	78 77 72 76 77	.0047 .0047 .0048	.4578 .4693 .4736	65 66 65
	12	UNC	.4720	83.6	.4843	72.2		.4688 .4688 .4844	87	.0048	.4736	62 68
1	16	UN	. 4950	83.1	.5040	72.1	(1)4 (1)4 (1)4 (1)4 (1)4 (1)4 (1)4 (1)4	.5000	72 77	.0048	.5048	71
1	18	UNF	.5020	83.8	.5106	71.9	0.5082	.5000 .5000 .5062	87 78	.0048	.5110 ]	50 71
	20 24	UN UNEF	.5090 .5170	83.9 84.1	.5162 .5244	71.3 70.4	112 [12]	.5156	72 87	.0048	.5204	65 78
.5625	43	UNUN	.5240	83.0 82.5	.5301	69.8 69.2	10.5203 0.5263	.5203 .5263 .5312	78 78 77	.0048 .0049 .0049	.5251 .5312 .5361	69 67 65

#### TABLE II.A.2 - Tap drill sizes, Unified screw threads, class 38 - continued

See footnotes at end of table.

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			Class 3	B minor diam	eter , interna	threads		Tap	drill and pe	rcent of three	ıd	
Thread size	Threads per inch	Desig – nation	Minimum	Percent of Thread	Maximum	1/ Percent of Thread	Drill	size	1/ Percent of Thread	Probable oversize, mean	Probable hole size	Percent 1/ of Thread
in 625 625 625 625 625 625 625 625 625	11 12 16 18 20 24 28 32	UNC UN UNF UNF UNEF UN UN	in .5270 .5350 .5570 .5650 .5710 .5800 .5860 .5910	83.0 83.1 83.8 83.1 83.1 83.1 83.1 83.1 83.8	in 5391 5662 5730 5787 5869 5926 5926	72.7 72.7 72.4 72.1 71.3 70.4 69.8 69.2	$\begin{array}{c} in \\ 17_{21} \\ 33_{44} \\ 9_{16} \\ 9_{56} \\ 0.5687 \\ 11_{44} \\ 0.5828 \\ 0.5828 \\ 0.5828 \\ 19_{22} \end{array}$	in .5312 .5469 .5625 .5687 .5781 .5781 .5781 .5828 .5828 .5828 .5938	79 72 77 78 78 72 87 78 72 87 78 91 77	in .0049 .0049 .0049 .0049 .0049 .0049 .0049 .0049 .0049 .0049 .0049	in 5361 5518 5674 5736 5830 5830 5830 5877 5877 5987	75 68 71 80 71 65 78 69 80 65
.6875 .6875 .6875 .6875 .6875 .6875 .6875	12 16 20 24 28 32	UN UN UNEF UN UN	.5970 .6200 .6330 .6420 .6490 .6540	83.6 83.1 83.9 84.1 83.0 82.5	.6085 .6284 .6412 .6494 .6551 .6594	73.0 72.8 71.3 70.4 69.8 69.2	<sup>19</sup> /2 5/8 41/4 41/4 16.5 mm <sup>21</sup> /2	. 5938 . 6250 . 6406 . 6406 . 6496 . 6562	87 77 72 87 82 77	.0049 .0050 .0050 .0050 .0050 .0050	.5987 .6300 .6456 .6456 .6546 .6546 .6612	82 71 65 77 71 65
.750 .750 .750 .750 .750 .750 .750 .750	10 12 16 20 28 32	UNC UNF UNF UNEF UN UN	.6420 .6600 .6820 .6960 .7110 .7160	83.1 83.1 83.8 83.1 84.1 84.1 83.8	.6545 .6707 .6908 .7037 .7176 .7219	73.5 73.3 72.9 71.3 69.8 69.2	<sup>41</sup> /4 <sup>21</sup> /2 <sup>11</sup> /16 <sup>45</sup> /4 18 mm <sup>23</sup> /2	.6406 .6562 .6875 .7031 .7087 .7188	84 87 77 72 89 77	.0050 .0050 .0050 .0051 .0051 .0051	.6456 .6612 .6925 .7082 .7138 .7239	80 82 71 64 78 64
.8125 .8125 .8125 .8125 .8125 .8125		UN UN UNEF UN UN	.7220 .7450 .7580 .7740 .7790	83.6 83.1 83.9 83.0 83.0 82.5	.7329 .7533 .7662 .7801 .7844	73.5 72.9 71.3 69.8 69.2	18.5 mm 34 <sup>49</sup> 54 19.75 mm <sup>25</sup> 52	.7283 .7500 .7656 .7776 .7812	78 77 72 75 75 77	.0051 .0052 .0052 .0052 .0052	.7334 .7552 .7708 .7828 .7864	73 71 64 64 64
.875 .875 .875 .875 .875 .875 .875 .875	9 12 14 16 20 28 32	UNC UN UNF UN UNEF UN UN	.7550 .7850 .7980 .8070 .8210 .8360 .8360 .8410	83.1 83.1 83.0 83.8 83.1 84.1 83.8	.7681 .7952 .8068 .8158 .8287 .8426 .8469	74.1 73.7 73.5 72.9 71.3 69.2	$ \begin{array}{c} {}^{49} 44 \\ {}^{25} / 42 \\ {}^{51} / 44 \\ 0.8024 \\ {}^{13} / 66 \\ {}^{53} / 64 \\ 21.25 \text{ mm} \\ {}^{27} / 42 \end{array} $	.7656 .7812 .7969 .8024 .8125 .8281 .8366 .8438	76 87 84 78 77 72 83 77	.0052 .0053 .0054 .0054	.7708 .7864 .8021 .8076 .8178 .8335 .8420 .8493	72 82 79 73 70 64 71 83
.9375 .9375 .9375 .9375 .9375 .9375	12 16 20 28	UN UN UNEF UN UN		83.6 83.1 83.9 83.0 83.0 82.5	.8575 .8783 .8912 .9051	73.9 72.9 71.3 69.8 69.2	22.75 mm	.8438 .8750 .8906 .8957 .9062	77 72 90 77	.0057 .0059 .0060	.8493 .8807 .8965 .9017 .9122	81 70 63 77 62
1.000 1.000 1.000 1.000 1.000 1.000	8 12 14 16 20 28 32	UNC UNF UNS UN UNEF UN UN	.8650 .9100 .9230 .9320	83.1 83.1 83.0 83.6 83.1 84.1 83.8	.9198 .9315 .9408 .9537 .9676	73.8 72.9 71.3 69.8	15/18 61/4	.8594 .8750 .9062 .9219 .9274 .9375 .9531 .9645 .9688	87 77 87 84 78 78 78 77 72 77 72 77	.0059 .0060 .0060 .0061 .0062 .0063 .0064	.8653 .8809 .9122 .9279 .9335 .9437 .9594 .9709 .9753	83 73 81 78 72 69 63 63 63 61
1.062 1.062 1.062 1.062 1.062 1.062	5 12 5 16 5 18 5 20	UN UN UN UNEI UN UN	.9270 .9720 .9950 1.0020 1.0080 1.0240	83.0 83.1 83.8 83.9	.9823 1.0033 1.0105 1.0162	74.1 72.9 72.1 71.3	$ \begin{array}{c} 13_{16}\\ 31_{22}\\ 1\\ 1\\ 1\\ 1^{1}_{164} \end{array} $	.9216 .9274 .9373 .9683 1.0000 1.0000 1.0150 1.0312		.0061           .0062           .0065           .0069           .0069           .0069           .0069           .0069	$\begin{array}{r} .9279\\ .9335\\ .9437\\ .9753\\ 1.0069\\ 1.0069\\ 1.0226\\ 1.0383\end{array}$	83 79 73 81 68 77 61 52
1.125 1.125 1.125 1.125 1.125 1.125 1.125	8 12 16	UNC UN UNF UN UNE	.9900 1.0350 1.0570	83. 83. 83.	1.0047 1.0448 1.0658	74. 74. 72.		.968 .984 1.000 1.031 1.062 1.062	4 70 0 71 2 81 5 71	3 .0067 7 .0069 7 .0071 7 .0074	.9750 .9911 1.0069 1.0383 1.0699	81 72 73 80 68
$1.125 \\ 1.125$	20 28	· UN UN	1.0710	83. 84.	1.078		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.078				
1.187 1.187 1.187 1.187 1.187 1.187 1.187	5 8 5 12 5 16 5 18 5 20	UN UN UNE UNE UN UN	1.0520 1.0970 1.1200 F 1.1270 1.1330 1.1490	83.           83.           83.           83.           83.           83.           83.	B         1.107           1         1.128           8         1.135           9         1.141	3         74.           3         72.           5         72.           2         71.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.062 1.093 1.125 1.125 1.140 1.151	8 8 0 7 0 8 6 7	7 7  7  7 		
$1.250 \\ 1.25$	7 8 12 16 16 18 20	UNC UN UNI UN UNE UN UN	1.1150 1.160 1.182	0     83.       0     83.       0     83.       0     83.       0     83.       0     83.       0     83.       0     83.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7 74. 8 74. 8 72. 0 72. 7 71.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.093 1.125 1.156 1.187 1.187 1.203 1.210	0 7 2 8 5 7 5 8	7 7 2		

TABLE II.A.2 — Tap drill sizes, Unified screw threads , class 3B - continued

See footnotes at end of table.

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TABLE II.A.2 - Top drill sizes, Unified screw threads, class 3B - continued

	_		Closs 3	38 minor dian	neter, interna	l threads		Top	drill and p	ercent of th	boen	
Thread size	Threads per inch	Desig— nation	Minimum	Percent of Thread	Maximum	Percent <sup>1</sup> / of Thread	Drill	5i20	Percent of Thread	Probable oversize, mean	Probable hote size	Percent of Thread
	1	1	in		in		in	l in		in	in	1
1.3125	8	UN	1.1770	83.4	1.1922	74.1	1/14/2	1.1719	87 77			
1.3125	12	UN	1.2220	83.6	1.2323	74.1	1%	1.1875	87			
1.3125	16	ŪN	1.2450	83.1	1.2533	72.9 72.1		1.2500	77			
1.3125	18 20	UNEF	1.2520	83.8 83.9	1.2605	72.1	162	1.2500	87 72			
1.3125	28	UN	1.2740	83.0	1.2801	69.8	32.5 mm	1.2795	71			
		1					(1)2	1.1875	87			
1.375	6	UNC	1.1950	83.1	1.2146	74.1	11% 11%	1.2031	79			
1.375	8	UN	1.2400	83.1	1.2547	74.1		1.2344	87 77			
1.375	12	UNF	1.2850	83.1	1.2948	74.1	1%	1.2812	87			
1.375	16	UN	1.3070	83.8	1.3158	72.9 72.1	1%	1.3125	77 87			
1.375 1.375	18 20	UNEF	1.3150 1.3210	83.1 83.1	1.3230	71.3	114	1.3281	72			
1.375	28	UN	1.3360	84.1	1.3426	69.8	34 m m	1.3386	78			
1.4375	6	UN	1.2570	83.4	1.2771	74.1	1174	1.2656	79	·		
1.4375	8	UN	1.3020	83.4	1.3172	74.1	11124	1.2969	87			
	12	UN	1.3470	83.6	1.3573	74.1	11%	1.3125	77 87			
1.4375 1.4375	16	Î ÛN	1.3700	83.1	1.3783	72.9	134	1.3750	77			
1.4375	18	UNEF	1.3770	83.8	1.3855	72.1	13% 13% 12%	1.3750	87 72			
1.4375	20 28	UN UN	1.3830	83.9 83.0	1.3912	71.3 69.8	35.5 mm	1.3906	88			
			1					1		1		
1.500	6	UNC	1.3200	83.1	1.3396	74.1	11% 11%	1.3125	87 79			
1 600	8	1157	1 2850	83.1	1.3797	74.1	ling	1.3594	87			
1.500		UN	1.3650	83.1	1	74.1	1126	1.3750	77 87			
1.500 1.500	12 16	UNF UN	1.4100	83.8	1.4198	74.1 72.9	11/2	1.4375	77			
1.500	18	UNEF	1.4400	83.1	1.4480	72.1	11/2 11/2 11/2	1.4375	87 72			
1.500	20 28	UN UN	1.4460	83.1 84.1	1.4537	71.3 69.8	37 mm	1.4531 1.4567	93			
		1		1				1				
1.5625	6	UN	1.3820	83.4	1.4021	74.1	1112	1.3906	79 87			
1.5625	8	UN	1.4270	83.4	1.4422	74.1	liz	1.4375	77			
1.5625	12 16		1.4720	83.6 83.1	1.4823	74.1 72.9	1.26	1.4688	87 77			
1.5625	18	UNEF	1.5020	83.8	1.5105	72.1	111/2 111/2 111/2 111/2 111/2 111/2 111/2	1.5000	87			
1.5625	20	UN	1.5080	83.9	1.5162	71.3	19%	1.5156	72			
1.625	6	UN	1.4450	83.1	1.4646	74.1	174	1.4531	79			
1.625	8	UN	1.4900	83.1	1.5047	74.1	(11)	1.4844	87			
1.625	12	UN	1.5350	83.1	1.5448	74.1		1.5000	77			
1.625	16	UN	1.5570	83.8	1.5658	72.9	1%	1.5625	.87 .77			
1.625 1.625	18 20	UNEF	1.5650	83.1 83.1	1.5730	72.1	194 194 194	1.5625	87			
1.040			1.5/10		1.5757		1		1		1	
1.6875	6	UN	1.5070	83.4	1.5271	74.1	(12 <u>2</u>	1.5000	87 79			
1.6875	8	UN	1.5520	83.4	1.5672	74.1	1%	1.5625	77			
1.6875	12	ÛN	1.5970	83.6	1.6073	74.1	11%	1.5938	87			
1.6875	16 18	UNEF	1.6200	83.1 83.8	1.6283	72.9 72.1	196	1.6250	77 87			
1.6875	20	UN	1.6330	83.8 83.9	1.6412	71.3	144	1.6406	72			
	_					I	10%	1.5312	84			
1.750	5	UNC	1.5340	83.1	1.5575	74.1	1122	1.5469	78			
1.750	6	UN	1.5700	83.1	1.5896	74.1		1.5625	87 79			
1.750	8	UN	1.6150	83.1	1.6297	74.1	livz	1.6094	87 77			
1.750	12	-	1		1		11%	1.6250	77			
1.750	16	UN UN	1.6600	83.1 83.8	1.6698	74.1 72.9	11/2	1.6875	87			
1.750	20	ŪN	1.6960	83.1	1.7037	71.3	1%	1.7031	72		.	
1.8125	_		1 0000			l	11.56	1.6250	87		<b>.</b>	
	6	אט	1.6320	83.4	1.6521	74.1		1.6406	79			
1.8125	8	UN	1.6770	83.4	1.6922	74.1	102	1.6719	87			
1.8125	12	UN	1.7220	83.6	1.7323	74.1	11/6	1.7188	79 87 77 87 77			
1.8125 1.8125	16 20	UN UN	1.7450	83.1 83.9	1.7533	72.9 71.3	1%	1.7500	77			
					1						1	1
1.875 1.875	6 8	UN UN	1.6950	83.1 83.1	1.7146	74.1		1.7031	79		.	
1.875	12	UN	1.7850	83.1	1.7948	74.1	144 144 186 196	1.7812	87			
1.875	16 20	UN UN	1.8070	83.8	1.8158	72.9	112	1.8125	77			
	-		1.8210	83.1	1.8287	71.3	1-54	1.8281				
1.9375	6	UN	1.7570	83.4	1.7771	74.1	194	1.7658	79			
1.9375	8	UN	1.8020	83.4	1.8172	74.1	1112	1.7969	87			
1.9375	12	UN	1.8470	83.6	1.8573	74.1	1176	1.8438	87 77 87 77 72			
		UN	1.8700	e 8/2 1	1.8783	72.9	114	1.8750	1 77	1	1	1
1.9375	16 20	UN	1.8830	83.1 83.9	1.8912	71.3	1 1 1 2	1.8906	90			

See footnotes at end of table.

·				Е Ш.А.2 —	Tup unit s	1265, 011116	D SCREW THREE				<u> </u>	
	Threads		Class 3	B minor diame	ter, internal			Тар	drill and pe	rcant of thre	ad	······································
Thread size	inreads per inch	Desi <b>g</b> – nation	Minlmum	Percent of Thread	Maximum	Percent of Thread	Drill	size	Percent of Thread	Probable oversize, mean	Probabla hole size	Percent 1/ of Thread
in 2.000 2.000 2.000 2.000 2.000 2.000	4.5 6 8 12 16	UNC UN UN UN UN UN	in 1.7590 1.8200 1.8650 1.9100 1.9320	83.5 83.1 83.1 83.1 83.1 83.8	in 1.7861 1.8396 1.8797 1.9198 1.9408	74.1 74.1 74.1 74.1 72.9 71.3	in 1 <sup>15</sup> /15 1 <sup>85</sup> /16 1 <sup>78</sup> 1 <sup>25</sup> /16 1 <sup>15</sup> /16 1 <sup>61</sup> /14	in 1.7812 1.8281 1.8750 1.9062 1.9375 1.9531	78 79 77 87 77 72			
2.000 2.0625 2.125 2.125 2.125 2.125 2.125	20 16 8 12 16	UNS UN UN UN	1.9460 1.9950 1.9450 1.9900 2.0350 2.0570	83.1 83.1 83.1 83.1 83.1 83.1 83.8	1.9537 2.0033 1.9846 2.0047 2.0448 2.0658	72.9 74.1 74.1 74.1 74.1 72.9	2 1 <sup>61</sup> /6 2 2 <sup>1</sup> /2 2 <sup>1</sup> /2	2.0000 1.9531 2.0000 2.0312 2 0625	77 79 77 87 77			
2.125 2.1875	20 16	UN UN UNS	2.0710	83.8 83.1 83.1	2.0787 2.1283	71.3 72.9	21/13 21/8	2.0625 2.1250	96 77			
2.250 2.250 2.250 2.250 2.250 2.250 2.250 2.250	4.5 6 8 12 16 20	UNC UN UN UN UN UN	2.0090 2.0700 2.1150 2.1600 2.1820 2.1960	83.5 83.1 83.1 83.1 83.8 83.8 83.1	2.0361 2.0896 2.1297 2.1698 2.1908 2.2037	74.1 74.1 74.1 74.1 72.9 71.3	{2 2 2 2 5 2 5 4 2 5 4 2 5 4 2 5 4 2 5 4 2 5 4 2 5 4 2 5 4 2 5 4 2 5 4 2 5 4 5 2 5 4 5 2 5 4 5 2 5 4 5 2 5 4 5 5 5 5	2.0000 2.0312 2.0625 2.1250 2.1562 2.1875 2.1875 2.1875	87 76 87 77 87 77 96			
2.3125	16	UNS	2.2450	83.1	2,2533	72.9	21/4	2.2500	77			
2.375 2.375 2.375 2.375 2.375 2.375	6 8 12 16 20	UN UN UN UN UN	2.1950 2.2400 2.2850 2.3070 2.3210	83.1 83.1 83.1 83.8 83.1	2.2146 2.2547 2.2948 2.3158 2.3287	74.1 74.1 74.1 72.9 71.3	23/18 21/4 58 mm 25/18 25/18	2.1875 2.2500 2.2835 2.3125 2.3125	87 77 85 77 96			
2.4375	16	UNS	2.3700	83.1	2.3783	72.9	23%	2,3750	77			
2,500 2,500 2,500 2,500 2,500 2,500 2,500	4 6 8 12 16 20	UNC UN UN UN UN UN	2.2290 2.3200 2.3650 2.4100 2.4320 2.4460	83.4 83.1 83.1 83.1 83.1 83.8 83.1	2.2594 2.3396 2.3797 2.4198 2.4408 2.4408 2.4537	74.1 74.1 74.1 74.1 72.9 71.3	$\begin{cases} 2^{7} 42 \\ 2^{1} 42 \\ 2^{3} 42 \\ 2^{3} 42 \\ 2^{3} 42 \\ 2^{3} 42 \\ 2^{7} 4$	2.2188 2.2500 2.3126 2.3750 2.4062 2.4375 2.4375	87 77 87 77 87 77 96			
2.625 2.625 2.625 2.625 2.625 2.625 2.625	4 6 8 12 16 20	UN UN UN UN UN UN	2.3540 2.4450 2.4900 2.5350 2.5570 2.5710	83.4 83.1 83.1 83.1 83.8 83.8 83.1	2.3844 2.4646 2.5047 2.5448 2.5658 2.5787	74.1 74.1 74.1 74.1 72.9 71.3	(211,42 23% 21,46 23,5 211,42 2 <sup>1</sup> ,46 2 <sup>9</sup> ,46 2 <sup>9</sup> ,46	2.3438 2.3750 2.4375 2.5000 2.5312 2.5625 2.5625	87 77 87 77 87 77 96			
2.750 2.750 2.750 2.750 2.750 2.750 2.750	4 8 12 16 20	UNC UN UN UN UN UN	2.4790 2.5700 2.6150 2.6600 2.6820 2.6960	83.4 83.1 83.1 83.1 83.8 83.8 83.1	2.5094 2.5896 2.6297 2.6698 2.6908 2.7037	74.1 74.1 74.1 74.1 72.9 71.3	212 2% 25% 2 <sup>11</sup> /11 2 <sup>11</sup> /15 2 <sup>11</sup> /15	$\begin{array}{c} 2.5000\\ 2.5625\\ 2.6250\\ 2.6562\\ 2.6875\\ 2.6875\\ 2.6875\end{array}$	77 87 77 87 77 96			
2.875 2.875 2.875 2.875 2.875 2.875 2.875	4 6 8 12 16 20	UN UN UN UN UN	2.6040 2.6950 2.7400 2.7850 2.8070 2.8210	83.4 83.1 83.1 83.1 83.8 83.8 83.1	2.6344 2.7146 2.7547 2.7948 2.8158 2.8287	74.1 74.1 74.1 74.1 72.9 71.3	25% 211/16 234 225/25 213/25 213/25	2.6250 2.6875 2.7500 2.7812 2.8125 2.8125	77 87 77 87 77 96			
3.000 3.000 3.000 3.000 3.000 3.000 3.000	4 6 8 12 16 20	UNC UN UN UN UN UN	2.7290 2.8200 2.8650 2.9100 2.9320 2.9460	83.4 83.1 83.1 83.1 83.8 83.8 83.1	2.7594 2.8396 2.8797 2.9198 2.9408 2.9537	74.1 74.1 74.1 74.1 72.9 71.3	234 2 <sup>13</sup> / <sub>16</sub> 278 74 mm 2 <sup>15</sup> / <sub>16</sub> -2 <sup>15</sup> / <sub>16</sub>	2.7500 2.8125 2.8750 2.9134 2.9375 2.9375	77 87 77 80 77 96			
3.250	4	UNC	2.9790	83.4	3.0094	74.1	3	3.0000	77		-	
3.500 3.750	4	UNC	3.2290 3.4790	83.4 83.4	3.2594 3:5094	74.1 74.1	3¼ 3¼	3.2500 3.5000	77			

TABLE II.A.2 - Tap drill sizes, Unified screw threads, class 3B - continued

1/ 100% of thread = 0.75H (see 20.2.3).

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TABLE II. A.3 - Recommended hole size limits before threading for different lengths of engagement, standard Unified and some UNS threads,

		Minor	closses 1 diameter of	closses 1B and 2B (see 30.1) Mixed alignments of Internet Internets	see 30.1) <u>]</u> /		been and be differed to solve the start between and be the solve the solve solve solve the solve solv	its limits for	al terret		
Nominal size in inches and threads perinch	Series designation	Minimum	Percent	Masimum	Percent <sup>E/</sup>	To and Inclu	To and Including 0.33D	Above 0.350 thru 0.670	thru 0.67D	Above 0.67D thru 1.5D	thru 1.5D
			Thread		Thread	M I nimum	Maximum	Midmum	Maximum	Minimum	Maximum
T	2	£	4	ß	6	7	8	6	10	11	12
.060-80 or No. 0-80	AND	in 0.0465	83.1	ún 0.0514	0.63	in 0.0465	in 0.0:00	in 0.0479	in 0.0514	in 0.0479	0.0314
.073-94 or No. 1404 .073-72 or No. 1-72	UNF UNF	.0561	83.3 83.1	.0623	52.7	.0561	.0599	.0580	.0618	.0585	.0623
.086-56 or No. 2-56 .086-64 or No. 2-66	UNC	.0667 1690.	83.3 83.3	.0737 0733	53.0 12.7	.0667	.0705	.0580	.0724	.0699	.0753
.009-18 or No. 3-18 .009-50 or No. 3-50	UNC UNFC	.0794	83.5 83.2	.0843	0.63 0.63	.0764	.0804	.0785	.0825 .0848	.0805	.0845
.112-40 or No. 4-40 .112-48 or No. 4-48	CNC	.0849	80.4 81.5	.0939	65.7 66.2	.0849 .0894	.0894	.0012	.09160	.0894	.0939
.125-40 or No. 5-40 .125-44 or No. 5-44	UNC	.1004	83.4 83.3	.1062	67.9 67.9	.1001	.1020	.1000	1041	.1021	.1052
.138-32 or No. 6-32 .138-40 or No. 6-40	CNC	101	8.28	<b>*</b> 11:	1.95 58.5	<b>8</b>	601 112	113	.112	601. 110	611. 119
,104-32 or No. 8-32 ,164-38 or No. 8-38	CNC	130	8.13 8.13	.139	0.19 19	021- 134	.135	.132	.137	.134	.142
,190-24 ur No. 10-24 ,190-32 or Nu. 10-32	C4 NND	991. 991.	8.18 1.88	156	62.8 04.0	991. 1991	991 991	141.	.163	991. 1900	<b>164</b>
.216-24 of No. 12-24 .216-28 of No. 12-28 .216-32 of No. 12-32	CNC	.171 .177 .182	8.1 8.1 8.18	181 181 181 181 181 198 11	64.7 64.7 64.0	.171 .177 .182	.176 .182 .180	.173	181.	176	181. 186 1901 -
.2:0-20 or 1/4-20 .2:0-28 or 1/4-28 .2:0-32 or 1/4-32 .2:0-36 or 1/4-32	CUNE	211	8888 	220	66.2 64.7 66.5 66.5	211	202 216 220	.190 .213 .218 .218	218	2200	.220 .224 .226
.3125-48 or 5/16-18 .3125-20 or 6/16-20 .3125-24 or 5/16-24 .3125-28 or 5/16-28 .3125-32 or 5/16-32 .3125-30 or 5/16-32	UNC 20UN 28UN 28UN UNE	252 263 274 282 282	8.5.588888 8.5.5.58888 8.5.5.5 8.5.5 8.5.5 5.5	288 282 282 288 288 288 288 288 288 288	65.56 65.76 65.76 65.76 65.76 65.76 65.76 65.76 65.76 65.76 65.76 77 76 76 76 76 76 76 76 76 76 76 76 7	252 274 282 282 282	259 278 278 282 282 283	2210 2210 283 283 283 283 283 283 283 283 283 283	281	259 272 285 285 285	285 2770 2770 285 282 286 288
.375-10 or 3/8-16 .375-20 or 3/8-20 .375-24 or 3/8-28 .375-28 or 3/8-28 .375-28 or 3/8-35 .375-38 or 3/8-36	UNC 20UN 28UN UNEF UNS	321 320 336 341 341 341	38322232 8	321 346 346 346 357 346 357 357 357 357 357 357 357 357 357 357	66.55 64.7 64.7 64.7 64.0 7	3304 575 575 575 575 575 575 575 575 575 57				327 327 345 345 345 345 345 345	321 332 340 340 340 352
.4375-14 or 7/16-14 .4375-16 or 7/10-16 .4375-20 or 7/10-20 .4375-28 or 7/10-28 .4375-32 or 7/10-32	UNE NOUN NOUNE NOUNE		88888 	1107 3384 405 405 405 405 405 405 405 405 405 40	66.3 65.4 65.4 65.3	404 1380 1383 1383 1383 1383 1383 1383 1383			400 100 100 100 100 100 100 100 100 100		
.500-13 or 1/2-12 .500-13 or 1/2/13 .500-18 or 1/2-18 .500-28 or 1/2-28 .500-28 or 1/2-28 .500-23 or 1/2-23	UNS UNC UNF 32UN	410 417 432 446 466	83.1 83.1 83.8 83.8 83.8 83.8	-428 -446 -446 -467 -467 -470	66.5 66.5 66.5 66.5 66.2 64.7 64.7 64.0	410 417 4417 4417 4417 4416 401 401	410 470 470 470	.414 .413 .449 .449 .449 .468	4123 472 472	419 432 432 452 452 452 452 452 452 452 452	416 416 416 416 416 416 416 416 416
See footnotes at end of table.											

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ABLE II.A.3 – Recommended hole siz
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		Mino	Vinor diameter of internal threads	internal threa	crosses 1D ura 2D (see 00.1) - confinued		and hole	aira limita fac	difformt land	1111480 Bostomenundud hulu eine limite fordifforent leentte of enverement	tan
Nominal size in inches and threads per inch	Series designation		Percent 2/	/ē	Percont 2/	To and including 0.33D	ing 0.33D	Above 0.33D thru 0.67D	thru 0.67D	Above 0.67D thru 1.5D	thru 1.5D
	in a state of the		Thread	שחעועםאַ	or Thread	Minimum	Maximum	Minimum	Maximum	Minimum	Maximum
<b>1</b>	2	Э	4	2	9	۷.	ω	ი	0	11	12
.5625-12 or 9/16-12 .5625-16 or 9/16-15 .5625-16 or 9/16-16 .5625-20 or 9/16-20 .5625-24 or 9/16-24 .5625-24 or 9/16-23 .5625-32 or 9/16-32	UNC UNF 16UN 20UN 28UNF 32UN	<sup>17</sup> 495 495 502 508 508 517 524	88888888888888888888888888888888888888	in 515 520 532 533 533	00000000000000000000000000000000000000	in 472 502 508 517 517 524	11 481 502 514 528 522 522 522 528	tn 477 - 477 - 506 - 506 - 511 - 520 - 520 - 530	17 505 512 517 530 533	11 1481 509 514 528 528 528 532	14 509 515 520 533 533 538
.625-11 or 5/8-11 .225-12 or 5/8-12 .623-16 or 5/8-16 .623-18 or 5/8-18 .025 20 or 5/8 29 .025 28 or 5/8 29 .625-28 or 5/8-32 .625-32 or 5/8-32	UNC 12UN 16UN 16UN 20UN 28UN 32UN	527 533 5557 5557 5557 5557 5557 5557 55	88888888888888888888888888888888888888	555 571 572 587 587 595 595 595 595	666655 6655 6652 6452 1126 6452 6450 6450 6450 6450 6450 6450 6450 6450	527 535 557 565 565 571 586 580 580	536 544 571 577 595 595 595	5339 5544 5588 55744 5938 5938 593	541 548 568 574 587 587 587 597 597	536 544 551 571 585 585 585 585 585 585	546 571 571 578 578 599 599 599
. 687.5-12 or 11/16-12 . 687.5-16 or 11/16-16 . 687.5-18 or 11/16-16 . 687.5-20 or 11/16-20 . 687.5-24 or 11/16-24 . 687.5-32 or 11/16-22 . 687.5-32 or 11/16-32	12UN 16UN UNS 20UN 28UN 32UN	597 620 627 633 649 649 649	8888888888888 8888888888888 91-89-0-6	615 640 645 652 657 661	657.0 657.0 657.4 657.6 557.6 557.7	.597 .620 .627 .633 .649 .649	627 634 634 647 653 653	602 630 630 651 651 651 651		606 634 639 647 653 653	.615 .640 .645 .657 .657
750-10 or 3/4-10 750-12 or 3/4-12 750-18 or 3/4-16 750-18 or 3/4-16 750-20 or 3/4-20 750-20 or 3/4-20 750-20 or 3/4-22 750-32 or 3/4-32	UNC 12UN UNF UNS 28UN 32UN	642 660 682 696 696 696 711	8888888888 11811-18	663 678 696 703 707 720	67.0 665.5 65.1 64.7 64.7 64.7 0 64.7	642 660 682 696 696 711 711	655 669 696 702 716 720	.647 .664 .686 .693 .699 .713 .713	658 673 693 704 718 718	652 669 689 696 702 716 720	.663 678 696 707 720 724
.8125-12 or 13/16-12 .8125-16 or 13/16-16 .8125-18 or 13/16-18 .8125-20 or 13/16-20 .8125-32 or 13/16-22 .8125-32 or 13/16-32	12UN 16UN UNS 28UN 32UN	722 752 778 779 779	88888833. 90.08888888 90.088888888888888888 90.08888888888	740 7765 788 788 788 788	655.66 657.0 657.4 8 57.7 4 8 5 7 7 4 8 5 7 4 8 5 7 4 8 5 7 4 8 5 7 6 5 7 8 5 7 8 5 7 8 5 7 8 5 7 9 7 7 9 7 9 7 9 7 9 7 9 7 9 7 9 7 9	111222	751 759 764 764 764 758	727 748 761 761 776	736 755 762 780 780	731 752 759 764 778 778	740 765 770 782 786
875-9 or 7/8-9 875-12 or 7/8-14 875-14 or 7/8-14 875-18 or 7/8-16 875-18 or 7/8-16 875-28 or 7/8-20 875-23 or 7/8-20 875-32 or 7/8-28	UNC 12UN 12UN 12UN 10NS 10NS 28UN 32UN	897 897 897 897 897 892 892 892 892 892 892 892 892 892 892	888888888888 	803 803 814 821 832 845 845 845 845 845	666666655755 64221557552 64321557552	755 798 897 881 882 882 883 882 883 882 883 882 883 882 883 882 883 882 883 882 882	766 794 806 821 821 840 840 840 840 840 840	760 881 824 828 828 828 828 828 828 828 828 828	772 810 818 828 843 843	766 794 806 814 821 827 845 845	778 803 814 821 832 832 832 8328 8328 8328 8328 832
.9375-12 or 15/16-12 9375-16 or 15/16-16 9375-20 or 15/16-26 9375-22 or 15/16-28 9375-32 or 15/16-32	12UN 16UN 28UN 32UN		888888 50010		67.0 657.0 657.4 655.7 655.7	847 870 883 883 883 883 899	877 877 903 903	852 887 901 901 901	.880 .882 .905 .905	.856 .877 .903 .903	

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.880 .928 .938 .946 .957 .970		0.998 1.015 1.053 1.071 1.078 1.082 1.095	1.077 1.115 1.134 1.140 1.145	1.123 1.178 1.178 1.196 1.203 1.203	1.202 1.240 1.259 1.255 1.265 1.282	1.225 1.265 1.303 1.328 1.328 1.332 1.332	1.288 1.327 1.365 1.386 1.386 1.386 1.386	1.350 1.350 1.428 1.448 1.453 1.453	1.413 1.462 1.400 1.509 1.515 1.520
.877 .919 .931 .938 .946 .946 .946 .970	981 981 983 993 1.002 1.009 1.014	0.984	1.065 1.106 1.127 1.134 1.139	1.109 1.180 1.180 1.180 1.202	1.252 1.252 1.255 1.256	1.252	1.272 1.315 1.356 1.356 1.384 1.384 1.403	1.335 1.317 1.419 1.439 1.438 1.446 1.452	1.397 1.440 1.481 1.502 1.508 1.508
	.946 .988 .988 .005 1.012 1.012 1.030	0.991 0.991 1.068 1.068 1.068 1.080	1.071 1.111 1.130 1.142 1.142	1.116 1.134 1.173 1.193 1.204 1.204	1.196 1.236 1.255 1.255 1.262 1.282	1.218 1.258 1.258 1.318 1.318 1.330	1.280 1.381 1.381 1.380 1.380 1.382 1.382	1.343 1.384 1.423 1.449 1.468	1.405 1.446 1.486 1.505 1.517
871 914 938 943 943 963 963 963	.934 .977 .989 .988 .988 .988 .988 .988 .988	0.977 996 1.039 1.061 1.068	1.058 1.102 1.123 1.130 1.136	1.102 1.102 1.164 1.164 1.166 1.169 1.109	1.184 1.227 1.228 1.256 1.256	1.202 1.289 1.311 1.318 1.318 1.338	1.265 1.373 1.373 1.373 1.373 1.386 1.386 1.386 1.386	1.327 1.414 1.414 1.449 1.449	1.390 1.434 1.477 1.498 1.508
877 919 938 938 946 946 946 946 946 946 946 946 970		0.084	1.1065	1.109 1.127 1.169 1.189 1.189 1.202 1.202	1.190 1.231 1.259 1.259	1.250 1.252 1.314 1.321 1.321 1.320	1.372 1.356 1.356 1.377 1.389 1.389	1.410 1.410 1.410 1.440 1.452 1.452 1.452	1.307 1.440 1.502 1.502 1.502 1.502
885 910 923 932 940 961 961 960	.927 .972 .985 .995 1.002 1.008	0.970 990 1.035 1.035 1.035 1.085 1.086	1.052 1.097 1.120 1.127 1.133	1.095 1.115 1.115 1.116 1.182 1.180 1.198	1.177 1.222 1.245 1.252 1.252	1.105 1.285 1.285 1.307 1.315 1.315 1.336	1.357 1.377 1.377 1.377 1.383 1.383	1.320 1.365 1.410 1.432 1.440 1.440	1.382 1.427 1.472 1.508 1.508
668888867.7 66888888867.7 66888888888	898898888888 66989888 7.4	88999 8899 1791 1997 1997 1997 1997 1997	88.59 85.89 85.89 85.89 85.89 85.89 85.89 85.89 85.89 85.89 85.89 85.89 85.89 85.89 85.89 85.89 85.89 85.80	88.5 88.5 88.5 1.7 1.7	68.1 67.0 65.9 65.8 65.8 65.8 65.8	69.3 66.5 66.5 66.2 66.2 66.2	69.1 63.6 65.8 65.8 65.8 65.8	69.3 65.5 66.5 66.5 65.1 65.1 65.2 65.2	689.1 687.0 657.0 657.8 657.8
890 938 938 938 938 938 938 938 938 938 938		0.098 1.015 1.071 1.078 1.078 1.078 1.082	1.077 1.115 1.115 1.140 1.140	1.123 1.140 1.178 1.203 1.203 1.203	1.202 1.240 1.259 1.259 1.265 1.282	1.225 1.205 1.301 1.328 1.328 1.328	1.388 1.368 1.384 1.384 1.384 1.385 1.385 1.385		1.413 1.452 1.460 1.509 1.515
88888888888888888888888888888888888888	88888888 4631896	88888888 3	888888 ••-***	8883888 3	888888 •••28888	8888888 	888888888 440-800	8888888 	8888888 •••0-1-80
805 923 932 940 940 961 966	.927 .972 .985 .985 .985 .985 1.002 1.008	0.970 980 1.035 1.057 1.057 1.057 1.057 1.085	1,052 1.097 1.120 1.127 1.133	1.095 1.115 1.115 1.160 1.182 1.182 1.196 1.196	1.177 1.222 1.245 1.252 1.258 1.258	1.105 1.240 1.285 1.307 1.315 1.315 1.336	1.257 1.302 1.347 1.370 1.383 1.383	1.320 1.410 1.410 1.440 1.440 1.440	1.382 1.427 1.472 1.495 1.503 1.503
UNES SUCES SURES SURES	8UN 12UN 12UN 12UN 16UN 20UN 28UN	UNC BUN BUN BUN 20UN 28UN	8UN 12UN 16UN 20UN 28UN	UNC CNF BUN BUN 20UN 28UN	8UN 12UN 16UN 20UN 28UN	UNC BUN BUN BUN 20UN 28UN	6UN 8UN 12UN 16UN 20UN 28UN	UNC BUN BUN BUN 20UN 28UN	6UN 8UN 18UN 20UN 20UN
1.000-8 1.000-12 1.000-14 1.000-16 1.000-20 1.000-20 1.000-20	1.0625-8 1.0055-12 1.0025-14 1.0025-16 1.0025-20 1.0025-20	1.125-7 1.125-8 1.125-12 1.125-10 1.125-20 1.125-20 1.125-20	1.187.5-18 1.187.5-18 1.187.5-16 1.187.5-18 1.187.5-20 1.187.5-28	1,250-7 1,220-8 1,220-12 1,220-16 1,220-20 1,220-20	1,3125-8 1,3125-12 1,3125-16 1,3125-18 1,3125-20 1,3125-28	1.375-6 1.375-8 1.375-12 1.375-16 1.375-20 1.375-20 1.375-20	1,4375–6 1,4375–8 1,4375–12 1,4375–16 1,4375–20 1,4375–20 1,4375–20	1.500-6 1.500-8 1.500-12 1.500-18 1.500-18 1.500-28 1.500-28	1, 5625-6 1, 5625-6 1, 5625-12 1, 5625-16 1, 5625-16 1, 5625-20

See footnotes at end of table.

				classes 1B and 2B (see 30.1) 1	3 (see 30.1	) <u>1</u> /-continued	nued				
		Minor	djameter of j	Minor diameter of internal threads	ę	Recomm	iended hole s	ize limits for	different ler	Recommended hole size limits for different fengths of engagement	ement
Nominal size in inches and threads per inch	Series		Percent 2/	<u>\</u>	Percent 2/	To and including 0.33D	ing 0.33D	Above 0.330 thru 0.670	thru 0.67D	Above 0.67D thru 1.5D	thru i.5D
	Including	Minimum	or Thread	Maximum	or Thread	Minimum	Maximum	Minimum	Maximum	Minimum	Maximum
1	2	£	4	5	9	2	ω	თ	10	11	12
1.625-6 1.625-6 1.625-16 1.625-16 1.625-18 1.626-20	6UN 8UN 12UN 16UN 20UN	in 1.445 1.490 1.535 1.557 1.565 1.571	8888888 1118	in 1.475 1.515 1.553 1.571 1.571 1.578	6666667.7.3 667.7.3 665.5.7 665.5 7.3 665.5 7.3 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5	in 1.445 1.490 1.535 1.535 1.557 1.565 1.565	in 1.460 1.502 1.544 1.571 1.571	in 1.496 1.496 1.539 1.561 1.568 1.568	tn 1.468 1.568 1.548 1.548 1.568 1.574	in 1.502 1.544 1.544 1.544 1.577	in 1.475 1.516 1.553 1.578 1.578 1.582
1.6875-6 1.6875-8 1.6875-12 1.6875-16 1.6875-16 1.6875-18 1.6875-20	6UN 8UN 12UN 16UN 20UN	1.507 1.552 1.597 1.697 1.627 1.633	888888888 4401.889	1.538 1.577 1.615 1.634 1.640 1.645	68.1 65.9 65.9 65.8 65.8	1.552 1.552 1.597 1.620 1.633	1.522 1.565 1.666 1.634 1.639	1.515 1.558 1.658 1.602 1.623 1.636	1.530 1.571 1.611 1.630 1.630 1.637 1.642	1.522 1.565 1.665 1.606 1.634	1.538 1.577 1.615 1.615 1.634 1.634 1.640
1.750-5 1.750-6 1.750-6 1.750-16 1.750-16 1.750-16 1.750-20	UNC 6UN 8UN 12UN 20UN	1.534 1.570 1.615 1.615 1.682 1.682 1.696	8888888 	1.568 1.600 1.640 1.678 1.678 1.696	666667.13 6667.13 66667.13 6667.13 66667.13 66667.13 66667.13 6667.13 66667.13 6667.13 6667.13 6667.13 6677.13 6677.13 6677.13 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	1.534 1.570 1.680 1.680 1.682 1.682	1.550 1.550 1.627 1.669 1.689 1.702	1.542 1.577 1.621 1.684 1.684 1.699	1.559 1.559 1.634 1.673 1.673 1.693	1.550 1.585 1.627 1.689 1.669 1.669 1.702	1.568 1.600 1.600 1.640 1.678 1.696 1.707
1.8125-6 1.8125-8 1.8125-12 1.8125-16 1.8125-20	6UN 8UN 16UN 20UN	1.632 1.677 1.722 1.722 1.758	8833.44 833.64 833.64 833.68 835.68 855.68 8	1.663 1.702 1.740 1.759 1.770	69.1 68.1 67.0 65.9 65.4	1.632 1.677 1.722 1.745	1.647 1.690 1.731 1.752	1.640 1.684 1.727 1.748 1.748	1.655 1.696 1.736 1.755 1.755	1.647 1.690 1.731 1.752 1.752	1.663 1.702 1.740 1.759 1.770
1.875-6 1.875-8 1.875-12 1.875-12 1.875-20	6UN 8UN 12UN 20UN 20UN	1.695 1.740 1.785 1.807 1.821	888888 111888 111888 111	1.725 1.765 1.803 1.821 1.832	69 67.7 66.5 66.5 66.5	1.695 1.740 1.785 1.867 1.807	1.710 1.752 1.794 1.814	1.702 1.746 1.789 1.811 1.811	1.718 1.758 1.758 1.818 1.830	1.710 1.752 1.752 1.814 1.814 1.827	1.725 1.765 1.803 1.821 1.832
1.9375-6 1.9375-12 1.9375-12 1.9375-16 1.9375-20	6UN 8UN 12UN 20UN 20UN	1.757 1.802 1.847 1.847 1.883	8888888 44901.0	1.788 1.827 1.865 1.865 1.884	69.1 68.1 67.0 65.9 65.4	1.757 1.802 1.847 1.870 1.883	1.772 1.815 1.856 1.889	1.765 1.808 1.852 1.852 1.853 1.886	1.780 1.621 1.821 1.861 1.880 1.880	1.772 1.815 1.856 1.856 1.877 1.889	1.788 1.827 1.865 1.884 1.895
2.000-4.5 2.000-8 2.000-8 2.000-12 2.000-12 2.000-20	UNC 6UN 8UN 10UN 20UN	1.759 1.820 1.865 1.910 1.946	8888888 7.1.8.1.8.1.	1.795 1.850 1.8890 1.928 1.946	71.0 697.7 665.5 665.5 665.5 665.5 665.5	1.759 1.820 1.9855 1.910 1.932	1.777 1.835 1.877 1.919 1.939 1.952	1.768 1.827 1.914 1.936 1.936	1.786 1.843 1.923 1.923 1.954	1.777 1.835 1.877 1.919 1.939 1.952	1.795 1.850 1.850 1.928 1.946 1.946

TABLE II.A.3 - Recommended hole size limits before threading for different lengths of engagement, standard Unified and some UNS threads,

FED-STD-H28/2A

	1.968 1.960 1.975 2.008 2.002 2.015 2.014 2.015			2.036 2.027 2.045	2.2.18 2.248 2.267 2.608 2.408 2.517	2.008	the state of the state distances for location of associated to red decinding 0.3.0. Moreover the minimum volume for Innerties of
	1.952	2.021	2.123	2.018	2.230	2.130	011 0 m
7. M	1.000	5.01 10.2 10.2	2.127	2.027	2.248	2.748	to and helled
1.995	1.945	25.057 2.057	2.120	2.009	2.229	2.120	
02.9	00.3		0.5.0	0.17 60.3	71.7	71.7	too lood by
2.009	1.975	2.031	1, 2.134	5.100	2.207	3.017	
83.1	3333	533 	83.1		88	22	
1.995	1.990	5.057	2.120	2.009	2.479	2.729	
CNS	BUN BUN	SOCN STORE	CNS	CNC BCN		CCC	
2.0625-16	2.125-6 2.125-8	2.120-12 2.126-16 2.123-20	2.1875-16	2.250-4.5 2.250-0	2.700-4	3.200-4	

10 8U1 angagement greater than 0.330 in sizes 0.25 in and larger are adjusted so that the difforence between limits is nover texe than 0.0040 in. Far diamater -pitch combinations other than thase given in this table, see 30.2. ē the tug ing for lengths of engagement tolorances  $\underline{1}$  The differences between limits are squal to the minor diameter

Hale size limits for diameter – pitch combinations which do not appear in this tobis may be obtained by uco of values in this tobis provided there is a diameter – pitch combination in the table:

(1) with the same pitch and

.

(2) with a diamater that is less by an integral amount than the diameter of the diameter - pitch combination for which hote size values are desired. (NOTE: Values in the table for nominal sizes isse than 0.25 h, cannot be used for this purpase.)

EXAMPLE: To obtain the values for the 4.000-QUN - 18 or 28 thread, add 2.000 to values for the 2.000 -BUN thread shown in the table. These values would then become:

3.865, 3.877, 3.871, 3.884, 3.877, 3.690. The percentages of thread will remain unchanged. 2/ Based an values as raunded off in the preceding column. 100 percent of thread = 0.75M(see 20.2.3). 3/ Based an a length of engagement equal to the nominal diameter.

		Minor d	Minor diameter of internal	Į₽	eods	1	Recommended hole	size limits fo	size limits for different lengths	ngths of engagement	lement
Nominal size in inches	Series			<u>∕€</u>	<u>2</u> / Percent	To and including 0.33D	ding 0.33D	Above 0.33D thru 0.67D	thru 0.67D	Above 0.67D thru 1.5D	thru 1.5D
upul lad sobalut Duo	munubisan	Minimum	Thread	Maximum	of Thread	Minimum	Maximum	Minimum	Maximum	Minimum	Maximum
1	2	З.	4	5	9	7.	8	6	10	11	12
.060-80 or No. 0-80	UNF	1 <sup>n</sup> 0.0465	83.1	in 0.0514	53.0	in 0.0465	in 0.0500	0.0479	in 0.0514	17 0.0479	in 0.0514
.073-64 or No. 1-64 .073-72 or No. 1-72	UNC	.0561	83.3 83.1	.0623	52.7 52.7	.0580	.0599	.0580	.0618	.0585	.0623
.086-56 or No. 2-56 .086-64 or No. 2-64	UNC	.0667	83.2 83.3	.0737	53.0 52.7	.0667	.0705	.0686 .0707	.0724	.0699	.0737
.099-48 or No. 3-48 .099-56 or No. 3-56	UNC	.0764	83.5 83.5	.0845	53.6 53.9	.0764	.0804	.0785	.0825	.0805	.0845 .0865
.112-40 or No. 4-40 .112-48 or No. 4-48	UNC	.0849	83.4 83.5 83.5	.0939 .0968	55.7 56.2	.0849	.0931	.0871	.0916	.0894 .0931	.0939
.125-40 or No. 5-40 .125-44 or No. 5-44	UNC	.1004	83.4 83.3	.1062	57.9 57.9	.0979	.1020	.1000	.1041	.1021	.1062
.138-32 or No. 6-32 .138-40 or No. 6-40	UNC	.1040	83.8 83.1	.1140	59.1 59.7	.1040	1601.	.1066	1115	.1091	.1140
.164-32 or No. 8-32 .164-36 or No. 8-36	UNC	.1300	83.8 83.1	.1389	61.8 62.1	.1300	.1345	.1324 .1359	.1367	.1346	.1389
.190-24 or No. 10-24 .190-32 or No. 10-32	UNC	.1450	83.1 83.8	.1555	63.7 63.8	.1450	.1502	.1475	.1528	.1502	.1555/ /
.216-24 or No. 12-24 .216-28 or No. 12-28 .216-32 or No. 12-32	UNC UNF UNEF	.1710 .1770 .1820	83.1 84.1 83.8	.1807 .1857 .1895	65.3 65.3 65.3	.1710 .1770 .1820	.1758 .1815 .1858	.1733 .1794 .1841	.1782 .1836 .1877	.1758 .1815 .1859	.1807 .1857 .1895
.250-28 .250-28 .250-32 .250-38	UNC UNF UNEF	.1960 .2110 .2200	8888 1.1.888 1.1.888 1.1.888 1.1.88 1	.2067 .2190 .2229 .2258	66.7 66.8 66.8 66.8 67.1	.1960 .2110 .2160	.2013 .2152 .2196 .2229	.1986 .2131 .2172 .2203	2040 2171 2212 2243	.2013 .2150 .2189 .2189	.2067 .2190 .2229 .2258
.312518 .31225-20 .31225-28 .3125-28 .3125-32	UNC 20UN 28UN UNEF UNS	.2520 .2580 .2580 .2670 .2790 .2790	88888833 5501198	2630 2680 2754 2847 2847 2847	6666666666 8865666666666666666666666666	25520 2580 2580 2740 2790 2790	.2577 2632 2714 2772 2817 2817	.2551 .2608 .2749 .2749 .2792	.2604 2656 2734 2789 2789 2833 2863	2577 2632 2632 2767 2767 2807 2807 2837	.2630 2680 2754 2807 2847 2847
.375-16 .375-20 .375-28 .375-28 .375-32	20UNC 20UN 28UN UNEF UNEF	-3070 -3210 -3300 -3360 -3410 -3410 -3450	88888888 8.1.1.1.8.1.	.3182 .3297 .3372 .3469 .3469 .3469	70.0 69.8 69.8 69.8 69.8 69.8 69.8	.3070 .3210 .3200 .3360 .3410 .3450	.3127 .3253 .3336 .3336 .3395 .3341	.3101 .3231 .3314 .3314 .3370 .3450	.3155 .3275 .3354 .3410 .3410 .3455 .3490	3128 3253 3332 3332 3386 3429 3461	.3182 .3297 .3372 .3426 .3469 .3469
. 4375-14 4375-16 . 4375-20 . 4375-28 . 4375-32	UNC 16UN UNF 32UN		888888 82.5001.5	.3717 .3800 .3916 .4051 .4094	70.9 70.8 69.8 69.8 69.8		.3660 .3749 .3875 .4020	.3630 .3723 .3855 .3995 .4040	.3688 .3774 .3896 .4035 .4080	.3659 .3749 .3875 .3875 .4011 .4011	.3717 .3800 .3916 .4051 .4094

FED-STD-H28/2A

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4223 4419 4637 4676 4719		5391 5463 5463 5463 5463 5463 5463 5585 5585 5585 5585 5585	6085 6085 6186 6189 6199 6289 6289		.7320 .7533 .7663 .7663 .7662 .7661 .7801	. 7681 . 7058 . 8068 . 8158 . 8158 . 8230 . 8469 . 8469	.8575 .8783 .8912 .9051	.8797 .9188 .9188 .9480 .9480 .9587 .9710	
4160 4226 4871 4487 4679	4783 4984 5085 5204 5204 5204	5402 5402 5403 5403 5403 5828 5828 5828 5828 5828 5828 5828 582			.7276 .7490 .7564 .7761 .7761	.7000 .7900 .8023 .8115 .8115 .8388 .8388 .8388 .8388	8524 8740 8872 9011 9054	.8722 .9148 .9271 .9489 .9489 .9489 .9489 .9489	
4192 4254 4395 4517 4517 4680		5486 5410 5710 5710 5875 5875 5875 5875 5875 5875 5875 587	.6282 .6282 .6335 .6335 .6335 .6335 .6476 .6355 .6580		7303 7512 7512 7585 7642 7783 7783	7026 845 8137 8137 8137 82810 8187 8410 8455	.8550 8762 8892 9035 9035		
4128 4196 4477 4477 4820	4753 4971 5045 5102 5102 5186 5186 5245	.5379 .5377 .5376 .5376 .5377 .5378 .5370 .5870 .5870			.7780 .7780 .7780 .7780	.7580 .7874 .7874 .8004 .8004 .8169 .83770 .8415	.8499 8719 .8519 .8852 .8853 .8995	.8684 .9123 .9249 .9249 .9419 .9419 .9627	
4181 4325 4371 4486 4881	.4783 .4994 .6695 .5065 .5123 .5206 .5210 .5316	.5328 .5408 .5408 .5410 .5410 .5410 .5410 .5410 .5410 .5410 .5410 .5410 .5410 .5410 .5410 .5410 .5410 .5410 .5410 .5410 .5410 .54000 .54000 .54000 .54000 .54000 .54000 .54000 .54000 .540000 .540000 .540000000000	.6029 .6114 .6314 .6313 .6313 .64159 .6459 .6520	.6481 .6652 .6866 .6866 .6866 .6968 .6908 .7145	.7276 .7491 .7665 .7665 .7770 .7816	.7614 .7800 .8023 .8116 .8116 .8190 .8395 .8395	.8524 .8741 .8873 .9020	.8722 9148 9271 9286 9440 9440 9445 9645	
4170 4170 4170 4610 4610	4120 4920 5170 5170 5170 5240	22222 22222 22222 22222 22222 22222 2222	6420 6420 6420 6420 6420 6420 6420 6420	8888 8888 8888 8888 8888 8888 8888 8888 8888	77588 77588 77588 77588 77588 77588 77588 77588 77588 7758 7758 775 775	5222 2222 2222 2222 2222 2222 2222 222	8470 83200 89830 89930 80930 80930 80050 80000 80000 80000 80000 80000 80000 80000 80000 8	819-9-9-9-9-9-9-9-9-9-9-9-9-9-9-9-9-9-9-	
8.17.71 8.8 9.8 9.8 9.8 9.8 9.8 9.8 9.8 9.8 9.8	22 22 22 23 24 24 25 25 25 25 25 25 25 25 25 25 25 25 25	722.7 722.7 722.7 868.8	73.0 72.1 72.1 69.8 69.8 69.8	73.5 72.1 72.1 69.8 69.8 69.8	73.5 72.9 69.8 69.8	732.5 732.5 722.6 99.8 99.8 99.8 99.8 99.8	73.9 73.9 712.9 60.8 60.8	74.1 74.1 73.8 723.8 723.8 723.8 723.9 69.8 69.8 69.8	
4223 4284 4419 4419 4537 4078 4078	+843 5040 5106 5102 5162 5244 5301 5344		. 6085 6284 63584 6412 6412 6412 6551	.6545 .6707 .6908 .6908 .6980 .7037 .7176 .7176		7681 7681 8068 8158 8158 8230 8469 8469	.9094		
8888888 	888888888 6-666-02	88888888888 0.1.8.1.1.1.8	888888888 9.1891.03	88888888 	8888888 8.5888888 8.188903	888888888 	88888 9-1902	88888888888888888888888888888888888888	
.4100 .4170 .4170 .480 .480 .480	-4720 -4850 -6850 -5020 -5170 -5170 -5240 -5280	5370 5350 5550 5560 5560 5560 5560 5560 556			.7220 .7450 .7520 .7520 .7740 .7740	7550 7850 7880 8807 8807 88150 820 82150 8200 82150 82150 82150 82150 82	8470 8700 8830 8830 8830 8980 8980 8040	880.000 880.0000 880.0000 880.0000 880.0000 880.0000 880.0000 880.0000 800.00000 800.00000 800.00000000	
UNC UNC UNF 32UN 32UN	UNF 100 200N 280N 280N 280N 280N 280N	UNC 12UNC 12UNC 20UNP 28UNP 28UNP 28UNP 28UNP	2800 2800 2800 2800 2800 2800 2800 2800	UNC UNF UNS SBUN SBUN SBUN SBUN	12UN 18UN 28UN 32UN 32UN	UNC 12UN 12UN 12UN 12UN 28UN 32UN 32UN	12UN 16UN 28UN 32UN	UNF UNF UNB 28UNE 28UNE	
	. 8035-12 6623-16 6623-18 6623-18 6623-29 6623-28 . 6623-28	-025-11 625-12 625-18 625-20 625-28 625-28 625-33	. (877–12 (8677–16 (8675–18 (8675–28 (8675–28 (8675–22 (8675–23	.750-10 750-10 750-18 750-18 750-28 750-23	.8125-12 .8125-18 .8125-18 .8125-20 .8125-23 .8125-23	.875-9 875-12 875-14 875-16 875-20 875-22 875-32	. 9375-12 . 9375-16 . 8375-20 . 8375-28 . 8375-32	1.000-8 1.000-12 1.000-13 1.000-18 1.000-28 1.000-28	Bee footnotes at end of table.

			Minor dia	Minor diameter of internal threads	mal threads		Recommo	nded hole size	limits for dif	ferent length	Recommended hole size limits for different tengths of engagement	ont
2	Nominal size in inches			<u>2</u> / Percent	<u>اب</u>	2/ Percent	To and including	ing 0.33D	Above 0.33D thru0.67D	thru0.67D	Above 0.67D thru	thru 1.5D
	and threads per inch	designation	Minimum	of Thread	Maximum	of Thread	M i nimum	Maximum	Mintmum	Maximum	Minimum	Mozimum
	1	2	· E	4	5	6	7	. 8	6	10	11	12
	1.0625-8 1.0625-12 1.0625-14 1.0625-14 1.0625-16 1.0625-20 1.0625-20	800 800 1200 1200 1200 1200 1200 2000 2800 28	in .9720 .9720 .9850 .9850 .9850 1.0020 1.0020 1.0020	888888888888 4672-8000	in 9823 9823 9823 9840 1.0033 1.0162 1.0162 1.0301	722.9 722.9 69.8 722.9 69.8	11 9720 9720 9850 9850 9850 1.0080 1.0080 1.0080	10 9347 9773 9896 9896 9896 1.0065 1.0025 1.0270	in 9748 9748 9874 9874 9869 1.0044 1.0014 1.0102	ta 9798 9798 9798 1.0012 1.0012 1.0142 1.0142	11 9347 9773 9773 9896 9896 1.0064 1.0024 1.0221	47 9823 9823 9840 1.0033 1.0105 1.0105 1.0105 1.0301
·	1.125-7 1.125-8 1.125-18 1.125-18 1.125-18 1.125-28	UNC BUN BUN BUN BUN 28UN 28UN	0.9700 0.9700 0.0500 0.10 0.700 0.10 0.10 0.10 0.10 0.10 0	88888888 7.1.1.8.1.1.1	0.9875 1.0047 1.0448 1.0658 1.0730 1.0787 1.0787	74.1 74.1 72.9 72.1 72.1 89.8	0.9700 9900 1.0350 1.0570 1.0570 1.0710 1.0710	0.9790 .9972 1.0398 1.0616 1.0616 1.0748 1.0748	0.9747 .9934 1.0373 1.0594 1.05669 1.0669 1.0727 1.0727	0.9833 1.0009 1.0423 1.0423 1.0710 1.0710 1.0710	0.9789 .9978 1.0398 1.0615 1.0689 1.0689 1.0747 1.0886	0.9875 1.0047 1.0448 1.0658 1.0730 1.0730 1.0730
	1.1875-8 1.1875-12 1.1875-16 1.1875-16 1.1875-20 1.1875-22	8UN 12UN 16UN 20UN 28UN	1.0520 1.0970 1.1200 1.1270 1.1330 1.1490	8888888 89.0 49.0	1.0672 1.1073 1.1283 1.1355 1.1412 1.1551	74.1 72.9 72.1 72.1 69.8	1.0520 1.0970 1.1200 1.1270 1.1330 1.1490	1.0597 1.1023 1.1241 1.1315 1.1373 1.1520	1.0559 1.0998 1.1219 1.1294 1.1352 1.1495	1.0634 1.1048 1.1262 1.1335 1.1335 1.1535	1.0597 1.1023 1.1240 1.1314 1.1372 1.1511	1.0672 1.1073 1.1283 1.1355 1.1412 1.1551
	1.250-7 1.250-8 1.250-12 1.250-16 1.250-18 1.250-28	UNC BUN BUN BUN 20UN 28UN	1.0950 1.1150 1.1150 1.1600 1.1820 1.1900 1.1960 1.1960	8888888	1.1125 1.1297 1.1698 1.1908 1.1980 1.2037 1.2037	744.1 744.1 722.9 722.9 87.2 8 9.8 8 9.8	1.0950 1.1150 1.1600 1.1820 1.1900 1.1990	1.1040 1.1222 1.1648 1.1866 1.1940 1.1998 1.1998	1.0997 1.1184 1.1623 1.1623 1.1844 1.1919 1.1977 1.2020	1.1083 1.1259 1.1673 1.1887 1.1887 1.1960 1.2017 1.2160	1.1039 1.1223 1.1648 1.1865 1.1865 1.1885 1.1897 1.2136	1.1125 1.1297 1.1698 1.1980 1.2037 1.2176
	.3125-8 .3125-12 .3125-16 .3125-16 .3125-20 .3125-20	80N 12UN 16UN 20UN 28UN	1.1770 1.2220 1.2450 1.2520 1.2580 1.2740	88888888 46-890	1.1922 1.2323 1.2533 1.2605 1.2662 1.2801	74.1 72.9 72.9 72.1 72.1 69.8	1.1770 1.2220 1.2450 1.2580 1.2580 1.2740	1.1847 1.2273 1.2491 1.2565 1.2653 1.2623	1.1809 1.2248 1.2469 1.2469 1.2602 1.2602	1.1884 1.2298 1.2585 1.2585 1.2585 1.2585	1.1847 1.2273 1.22490 1.2564 1.2622 1.2761	1.1922 1.2533 1.2605 1.2662 1.2862
	1.375-6 1.375-18 1.375-12 1.375-18 1.375-18 1.375-28 1.375-28	UNC BUN BUN BUN COUN 280UN	1.1950 1.2850 1.2850 1.3070 1.3150 1.3210 1.3360	8888888 	1.2146 1.2547 1.2547 1.2548 1.3158 1.3287 1.3287 1.3287	74.1 74.1 72.9 72.1 72.1 80.8	1.1950 1.2400 1.2850 1.3070 1.3150 1.3360	1.2046 1.2472 1.2898 1.3116 1.3190 1.3248 1.3395	1.1996 1.2434 1.2873 1.3094 1.3169 1.3169 1.3227 1.3227	1.2096 1.2509 1.2509 1.3137 1.3137 1.3257 1.3257 1.3257	1.2046 1.2472 1.2898 1.3115 1.3189 1.3386 1.3386	1.2146 1.2547 1.2548 1.3158 1.3158 1.3287 1.3287
and the second	1.4375-4 1.4375-4 1.4375-12 1.4375-18 1.4375-18 1.4375-23 1.4375-23	6UN 8UN 12UN 20UN 28UN	1.2570 1.3020 1.3470 1.3770 1.3770 1.3830 1.3890	88888888 440-0000	1.2771 1.3772 1.3573 1.3783 1.3855 1.3855 1.3912 1.4051	74.1 74.1 72.9 71.3 71.3 71.3 69.8	1.3570 1.3720 1.3720 1.3770 1.3530 1.3530	1.2671 1.3097 1.3523 1.3741 1.3741 1.3815 1.3873 1.3873 1.4020	1.362 1.362 1.3496 1.3794 1.3794 1.3794 1.3852 1.3852	1.2721 1.3134 1.3548 1.3762 1.3835 1.3835 1.3835 1.3835	1.2671 1.3097 1.3529 1.35240 1.3814 1.3814 1.3872 1.3872 1.4011	1.2771 1.3172 1.3573 1.3783 1.3783 1.3855 1.3855 1.3855 1.3812
	1.500-6 1.500-8 1.500-12 1.500-16 1.500-16 1.500-20 1.500-28	UNC BUN BUN BUN 16UN 20UN 28UN	1.3200 1.3650 1.4100 1.4400 1.4400 1.4460 1.4460	333888888 1118111	1.3396 1.3797 1.4198 1.4408 1.4408 1.4480 1.4537 1.4537	74.1 74.1 72.1 72.1 89.8	1.3200 1.3650 1.4100 1.4400 1.4400 1.4460 1.4460	1.3296 1.3722 1.4148 1.4366 1.4440 1.4440 1.4495 1.4445	1.3246 1.4123 1.4123 1.4424 1.4477 1.4477 1.4477	1.3346 1.3759 1.4173 1.4387 1.4387 1.4460 1.4460 1.4517 1.4560	1.3296 1.3722 1.4148 1.4439 1.4439 1.4437 1.4437 1.4437	1.3396 1.3797 1.4198 1.4408 1.4480 1.4480 1.4537

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Based an a longth of ongogement oqual to the nominal diameter.

બુષ્ટ

(1) with the same pitch and (2) with a diameter that is less by an integral amount than the diameter - pitch combination for which hole also values are desired. (NOTE: Values in the table for nonlocil class less than 100 aroman be used to use 4. Control and the values for the 9.000-BUN-3B thread, add 2.000 to the values for the 2.000-BUN thread aboun in the table. Those values would then became: 3.8650, 3.8722, 3.8084, 3.8759, 3.8722, 4.6797, The parentages of thread will remain unchanged.

engagement greater than 0.330 in sizes 0.25 in. and larger are adjusted so that the difference between limits is never less than 0.0040 in. For diameter -pitch combinations

other than those given in this table, see 30.2.. Hole aize limits for diameter—pitch combinations which do not appear in this tablo may be obtained by use of values in this table provided there is a diametor -pitch.

combination in the table:

5

 $m \lambda/$  The differences batween limits are equal to the minor diameter tolerances for lengths of engagement to and including 0.33D. However, the minimum values for lengths

1.7146 1.7547 1.7948 1.8158

.7898 .8115 .8247

1.8137

1.8227

7472 7898 8116 8248

1.8210 1.7400 1.7850 1.8070

74.1

7547 7948 8158 8158

1.128.23

.7400 .7850 .8070 .8210

8UN 8UN 12UN 20UN

1.875-6 1.875-8 1.875-12 1.875-16 1.875-16

7146

7046

.7698

.7434

7046

1.6521 1.6922 1.7533 1.7662

.7273 .7273 .7490 .7622

1.72984 1.7298 1.7512 1.7642

6371 6809 7248 7169

.6421 .6847 .7273 .7273 .7491 .7623

74.1

.6320 .6770 .6770 .7220 .7220

8CN 8CN 12UN 20UN

1.8125-6 1.8125-8 1.8126-12 1.8125-16 1.8125-16

6521

6320

0421

1.8172 1.8573 1.8783 1.8912

8097 8523 8740 8872

1.8134 1.8548 1.8762 1.8892

1.7621 1.8059 1.8498 1.8710 1.8852

.8097 .8523 .8741 .8873

1.8470

74.1

1.7771 1.8172 1.8573 1.8573 1.8912

83.4 83.6 83.1 83.1 83.1 83.1

.7370 02470 8700 1.8830

8UN 8UN 12UN 18UN 20UN

1.9375-6 1.9375-8 1.9375-12 1.9375-12 1.9375-20

7671

7570

.777.

7671

7721

.7861 8793 8797 9198

.7728

7794

1992

.7727

2.0033

.0012

1.9969

1669.1

1.6930

72.9

2.0033

83.1

UNS

.0625-10

.9537

.9148 .9365 .9497 0680.1

.8340 .8759 .9173 .9387 .9517

.8246 .8684 .9123 .9344 .9344

8298 8722 9366 9366

74.1

1.9198

2801

8797

8888888 2.288888 2.288888

.000-4.5 .000-6 .000-8 .000-12 .000-12

1.9646 2.0047 2.0448 2.0858 2.0787

9546 9972 0398 0747

0596 0423 0637

1.0400 1.0934 2.0373 2.0594

9548 0398 0398 0748

1.9450 1.9450 2.0350 2.0350 2.0570

74.1

1.9846 2.0047 2.0658 2.0787

83.1 83.1 83.8 83.8

9450 9900 0350 0350

8UN 12UN 16UN 20UN

2.125-6 2.125-8 2.125-12 2.125-16 2.125-16 2.125-20

2.0381

0294

2.0227 2.0796

2.0090

2.0381

83.5 83.1

2.0090 2.0700

NNO 9 UNC UNS

2.250-4.5 2.250-8

2.1875-18

2.1283

2.1240 0228

2.1262

2.1219 1910.1

2.1241

2.1200

72.9 11.1

2.1283

83.1

2.1200

2.2594 2.5094 2.7694 3.0094

2444 4944 7444 9944

2519 5019 7519 0019

 $\begin{array}{c} \mathbf{2.2369}\\ \mathbf{2.4869}\\ \mathbf{2.7369}\\ \mathbf{2.7369}\\ \mathbf{2.0869}\\ \mathbf{2.0869}\end{array}$ 

2444 9444 9844

2.2200 2.4700 2.7280 2.0780

74.1

2594

83.4 83.4 83.4

2.22002.47902.72002.0790

.5575 .5896 .6297 .6698 1.6908

.5798 .6222 .6848 .6885 .6885

.5515 .5846 .5846 .6259 .6673 .6673

5395 5746 6184 6623 6844

.5455 .5796 .6222 .6868 .6888

74.1

.5575 .5896 .5896 .6297 1.6698 1.6698

CNC SUN 20UN 20UN 20UN

1.750-5 1.750-6 1.750-8 1.750-12 1.750-16

5455

5271 5672 6073 6283 6355 6412

5171 5597 6023 6240 6314 6314

1.5221 .5634 1.6048 1.6262 1.6335

1.6121 .5559 1.6998 1.6294 1.6294

5171 5597 5597 6023 6315 6315

1.6320 1.6200 1.6200

74.1

6073 6283 6355 6412

8888888

5070 5870 6270 6330

800N 800N 1120N 1600N 200N

.6875-6 6875-8 6875-12 .6875-12 .6875-13 .6875-18

5070

5271

4048 5047 5448 5448 5730 5730

1.4546 1.4972 1.5398 1.5615 1.5689 1.5747

4596 5637 5787 5787

5373 5594 5689 5727

4546 4972 5698 5690 5748

.4450 4900 5350 5350 5350 5570 5710

74.1

4646 5047 5448 5448 5488 5730 5730

83.1 83.1 83.1 83.1 83.1 83.1

4450 5350 55570 5650 5710

8UN 8UN 12UN 20UN 20UN

.625-6 .625-8 .625-12 .625-16 .625-18 .625-18

4498

4021 4422 4823 5033 5105

1.3921 1.4347 1.4773 1.4990 1.5064

3971 4384 4798 5012 5085 5142

4773 4991 5065 5123

74.1

4422 6033 5105 5105

83.9 83.9 83.9 83.9

3820 4270 5020 5080

8UN 8UN 18UN 18UN 20UN

5625-12 5625-16 5625-18 5625-18 5625-20

.4021



#### APPENDIX B

#### DESIGN OF UNIFIED SCREW THREADS

40. Scope. This appendix provides guidelines which may be used in the design of unified screw threads for threaded parts. It is not a mandatory part of the standard. The information contained herein is intended for guidance only. It supplements information contained in Appendix B of ANSI B1.1-1982.

50. General.

50.1 Introduction. In general, any given problem in thread design may be susceptible to several more or less satisfactory solutions based on the preliminary selection of certain elements of the design and the proper adjustment of the other elements. In other words, thread design is to a large extent empirical and is partially based on previous experience with similar designs and the judgment of the designer. Accordingly, it is not practicable to present a definite system of approach to the design of a threaded assembly but merely to present a discussion of various design factors.

50.2 Factor relationships. The interrelation of length of engagement, minimum major diameter of the external thread, maximum minor diameter of the internal thread, and the strength of the assembled thread needs to be understood and carefully considered in order to produce the optimum design of a special thread. It is not economical to use either a length of thread engagement which is longer than required or shorter than that which will develop the full strength of the externally threaded member. Other factors, such as control of tap breakage, proper seating of a threaded part on a shoulder, the prevention of cross threading, conditions of loading when the assembled parts are not concentric, and possible collapse of a hollow externally threaded member, require careful analysis and adjustment of the design with respect to selection of the diameter-pitch combination, the class of thread, length of engagement, and major and minor diameter tolerances.

50.3 Thread fit considerations. A close fitting thread assembly under some conditions may fail, whereas the cause of failure may be eliminated by providing a looser fit. A cap screw that seats only on one side of the bearing surface under the head may break off when the screw is tightened. When a screw has a large bearing surface under the head or when the head must be square with a projecting pin, sufficient pitch diameter clearance must be provided to allow for any out-of-squareness of the screw axis with the bearing surface under the head. Thus, as large a pitch diameter tolerance as possible, together with providing proper tolerances on squareness of face with the thread axis where seating is required, may avoid the necessity for specifying a heat treated bolt.

50.4 <u>Standard threads</u>. Use of standard threads is required in accordance with 4.1. Information on preferred sizes and classes for special threads ap-pears in 5.1 and 5.2. Whenever practicable, lengths of engagement for coarse, fine, 4,6 and 8 thread series should be between 5 pitches and 1 1/2 diameters; for all other series they should be between 5 and 15 pitches. Application of these principles will help keep costs of manufacture and gaging to a minimum.

## 60. Eccentricity of assembly and cross threading.

Note: Table 6 of ANSI B1.1-1982 includes tables of 0.375H, 0.75H and H.

In assembly and use, the combined tolerances and allowances on both mating parts should not allow threads to disengage on one side when assembly is eccentric. The axis of the internal thread can be displaced radially from coincidence with the axis of the external thread by an amount equal to the sum of the pitch diameter tolerances and the allowance. This radial displacement may be sufficient so that the flank contact is entirely on one side and on the opposite side the crest of the external thread will be in line with the crest of the internal thread with the following results when the screw is constrained in such a position in a tapped hole: (1) There will be danger of crossing the threads in starting, and (2) the screw may pull out of the hole when tension is exerted in this constrained position. The minimum amount of overlap is arbitrary and controversial, but the following general rule can be used in lieu of more specific data:

As the first step to assure the minimum safe overlap on both sides when the assembly is concentric, the difference between the minimum major diameter of the external thread and the maximum minor diameter of the internal thread should not be less than twice the addendum of the external thread (0.75H). Otherwise stated, the sum of the major-diameter tolerance and allowance, if any, of the external thread and the minor-diameter tolerance of the internal thread should not be greater than 4/3 the addendum of the external thread, 0.5H. This provides for a minimum of 50 percent thread engagement. As the second step, to assure the minimum safe overlap on one side when the assembly is eccentric, the difference between the maximum pitch diameter of the internal thread and the minimum pitch diameter of the external thread should not be greater than the basic thread height (0.625H). Otherwise stated, the sum of the pitch-diameter tolerances of both threads and the allowance, if any, should not be greater than the basic thread height (0.625H). This provides for an eccentric assembly condition equal to half the basic thread height (0.3125H) and zero minimum overlap on one side. If the results from the limits of size selected violate the above rules, the tolerances should be reduced by using a closer class of tolerance, assuming tolerances consistent with manufacturing possibility, or a coarser pitch should be used to increase the amount of overlap. The major-diameter tolerance of the external thread or minor-diameter tolerance of the internal thread should not be less than the pitch-diameter tolerance of the respective thread to maintain thread form. Also, it should be noted that, if the tolerance on the minor diameter of the internal thread must necessarily be large, the major diameter of the external thread must be held close to the maximum major diameter and vice versa.

#### 70. Strength factors.

70.1 Tensile stress area. Tests have shown that externally threaded parts fail in tension at loads corresponding to those of unthreaded parts with diameters midway between their pitch and minor diameters. Formulas (1a) and (1b) in table II.B.1 provide stress area based upon a diameter approximately midway between minimum pitch diameter and minimum minor diameter. These formulas have been applied successfully to steel and other metals with ultimate strengths up to 180,000 psi and are often used for product acceptance. Tensile stress areas for standard sizes are tabulated in section 11 of ANSI B1.1-1982.

70.2 Shear areas at minimum material. The geometric shear area of an internal thread at minimum material is equal to the area of that thread which is intersected by a cylinder with a diameter equal to the minimum major diameter of the mating external thread over the length of engagement. This is identified in figure 2.B.1 for a one pitch section and formulas (2a) and (2b) in table II.B.1 are used for calculation. Similarly, the geometric shear area of an external thread at minimum material is equal to the area of that thread which is intersected by a cylinder with a diameter equal to the maximum minor diameter of the mating internal thread. This is also identified in figure 2.B.1 for a one pitch section and formulas (4a) and (4b) in table II.B.1 are used for calculation.

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TABLE II.B.I FORMULAS FOR SUREW THREAD STRENGTH FACTORS				
FORMULA NUMBER	CHARACTERISTIC	FORMULA	REFERENCE	
(10)	Tensile Stress Area	$A_{\rm g} = 3.1416 \left( \frac{d_2 \text{bac}}{2} - \frac{3H}{16} \right)^2$	70.1	
(16)		$A_{\rm B} = 0.7854 \left( d  bsc - \frac{0.9743}{n} \right)^2$	70.1	
(2a)	Shear area, internal threads (Min material ext and int threads)	$AS_n min = 3.1416 n LE d_{min} \left[ \frac{1}{2n} + 0.57735 (d_{min} - D_2 max) \right]$	70.2	
(2b)		$AS_{n} \min = 3.1416 d_{min} \left[ 0.875 - 0.57735n \left( Td + TD_{2} + ss \right) \right] LE$	70.2	
(3)	Shear area, internal threads (Simplified: for d equal to or areater than 0.250 inch)	$AS_{h} = 3.1416 D_{2}bst \frac{3LE}{4}$	70.4	
(40)	Shear area, external threads (Min material ext and int threads)	$AS_{s} \min = 3.1416 \text{ n LE } D_{l} \max \left[ \frac{1}{2n} + 0.57735 \left( d_{2} \min - D_{l} \max \right) \right]$	70.2	
(4b)		AS <sub>s</sub> min = 3.1416 D <sub>1</sub> max $\left[ 0.75 - 0.57735n (TD1 + Td2 + es) \right] LE$	70.2	
(5)	Shear area, external threads (Simplified)	AS <sub>8</sub> = 3.1416 d2bsc 5/8 LE	70.4	
(60)	Shear area, external threads (Basic size ext and int threads)	AS <sub>8</sub> max = 3.1416 D <sub>1</sub> bsc $\frac{3}{4} \left( \frac{LE}{dbec} \text{ tram Fig 2.B.2} \right) d_{bsc}$	70.3	
(6b)		AS <sub>s</sub> max = 3.1416 Djbsc <u>3</u> LE	70.3	
(7)	Shear area, combined failure	$AS = 3.1416 D_2 bsc \frac{LE}{2}$	70.5	
(8)	Shear stress area ratio	R <sub>1</sub> = <u>Formula (60) or (6b)</u> Formula (2a) or (2b)	70.7.5	
(9)	Material strength ratio	$R_2 = \frac{UTS_n}{UTS_n}$	70.7.5	
		1		

TABLE 11.8.1	FORMULAS FOR	SCREW THREAD	STRENGTH FACTORS

Notation: d = major diameter, external thread (was  $D_8$ )

- $d_2$  = pitch diameter, external thread (was E<sub>8</sub>)
- $D_1 = minor diameter, internal thread (was K_n)$
- $D_2 = pitch diameter, internal thread (was E_p)$
- es = allowance, external thread (was G)
- LE = length of thread engagment (was Le)

n = number of threads per inch

 $\text{UTS}_n$  = ultimate tensile strength of internally threaded part

UTS<sub>8</sub> = ultimate tensile strength of externally threaded part

Td, Td<sub>2</sub>, TD<sub>1</sub>, TD<sub>2</sub>, = tolerance on d, d<sub>2</sub>, D<sub>1</sub>, D<sub>2</sub> respectively

 <u>3H</u>
 ,0.1875H = half external thread addendum

 16
 ,0.1875H = half external thread addendum

 (tabulated in Table 6 of ANSI B1.1 - 1982)

bsc,max,min = modifiers denoting basic,maximum and minimum values, cospectively Downloaded from http://www.everyspec.com

## FED-STD-H28/2A

FORMULA NUMBER	CHARACTERISTIC	FORMULA	REFERENCE PARAGRAPH
(11)	Tensile stress, externally threaded part — pure tension	$S_{t} = \frac{F}{A_{s}^{B}}$ from (1a) or (1b)	70.6
(12)	Combined tensile stress, externally threaded part	$S'_{1} = S'_{s} + \frac{S_{1}}{2}$	70.6
		with $S_{t} = \frac{F}{0.7854[(d_{1}min)^{2} - d_{h}^{2}]}$	
		$S'_{s} = \sqrt{\left(\frac{S_{t}}{2}\right)^{2} + \left(S_{s}\right)^{2}}$	
		$S_{g} = \frac{T \ d_{l} \min}{0.1963 \left[ \left( d_{l} \min \right)^{4} - d_{h}^{4} \right]}$	
(13)	Length of engagement based upon combined shear failure of external and internal threads	$LE = \frac{4A_{B}^{ix} \text{ from (1a) or (1b)}}{3.1416 d_{2} \text{ bsc}}$	70.7.3
(14)	Length of engagement based upon shear of external thread	LE = $\frac{2A_{B}^{*} \text{ from (1a) or (1b)}}{\frac{AS_{B} \text{ from (4a) or (4b)}}{LE}}$	70.7.4
(15)	Length of engagement based upon developing full tensile strength of external thread with threads at basic size—used with (IG)	$LE = \frac{2A_s^{\text{*}} \text{ from (1a) or (1b)}}{\frac{AS_s \text{ from (6b)}}{LE}}$	70.7.5
(16)	Length of engagement based upon shear of internal thread $\left(\frac{R_1}{R_2}\right)$ is greater than 1	LE = LE from(15) x $\frac{R_1 \text{ from (8)}}{R_2 \text{ from (9)}}$	70.7.5

TABLE II. B.2 FORMULAS FOR SCREW THREAD DESIGN

Notes: 1. Where  $A_s^*$  is indicated, subtract 0.7854df from  $A_s$  for a hollow part.

2. Numbers in parenthesis are formula numbers from Table II and from this table.

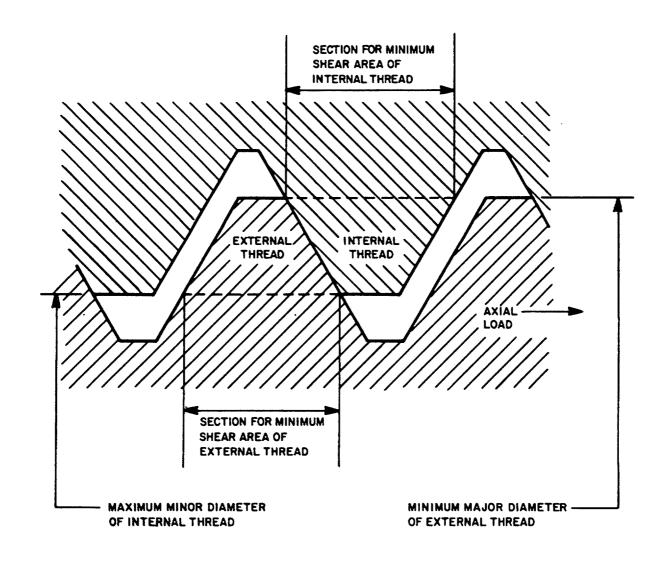
Notation  $d_1$ min = minimum minor diameter, external thread, flat form (was K<sub>s</sub>min), inch. In formula (12),  $d_1$ min =  $d_2$ bsc  $-\frac{3}{4}$ H =  $d_{bsc} - \frac{1.2990}{n}$ .

 $d_h$  = hole diameter, externally threaded part, inch. If there is no hole,  $d_h$  = 0

F = axial load on externally threaded part, Ib

S<sub>8</sub>=shear stress, psi

- S<sub>s</sub><sup>/</sup>=combined shear stress, psi
- T = transmitted wrench torque in threaded section(approximately half of the applied wrench torque), in.-1b.



#### FIGURE 2. B. I SHEAR AREAS AT MINIMUM MATERIAL

70.3 Shear areas at basic size. The geometric shear area of an external thread at basic size is equal to the area of a basic size thread which is intersected by a cylinder with a diameter equal to the basic minor diameter. Formulas (6a) and (6b) of table II.B.1 are used for calculation. The geometric shear area of an internal thread at basic size is not ordinarily used for calculations.

70.4 Shear area simplified formulas. Formulas (3) and (5) in table II.B.1 are simplified formulas for internal and external thread shear areas. They are based upon empirical data and give shear areas which vary from the geometric minimum material shear areas. In some cases, test data agrees more closely with these simplified formula shear areas than with geometric shear areas.

70.5 Shear area, combined failure of external and internal threads. When the mating external and internal threads are on parts manufactured from materials of approximately equal strength, failure will usually take place in both threads simultaneously. Thread bending during failure changes the thread geometry in this case so that effective shear area is significantly smaller than those calculated from formulas discussed in 70.2, 70.3 and 70.4 above. Formula (7) in table II.B.1 is an empirical formula which gives an approximate equivalent for this case. Numerically, it describes a failure at the pitch diameter of one of the threads.

70.6 Tensile stress. Formula (11) in table II.B.2 is often used for acceptance of externally threaded fasteners with ultimate tensile strength, yield strength, or some other selected stress level applied to  $S_t$  in order to determine the required axial test load. When threads are used in a joint, a tightening torque is applied to overcome friction under a bolt head or nut, to overcome thread friction, and to develop the axial load. This torque results in a shear stress, which when combined with the tensile stress from the axial load, causes an increase in the effective tensile stress. Formula (12) in table II.B.2 describes this situation. Experience has shown that for a solid externally threaded part, the combined stress is generally about 20% greater than the tensile stress calculated from formula (11). Therefore, in this case, the combined stress is often assumed to be 1.2S<sub>t</sub> or is not considered due to satisfactory experience with the Factor of Safety used.

### 70.7 Length of engagement, LE.

70.7.1 If failure of a fastening system using standard threaded fasteners should occur it is generally more economical that the externally threaded part will break rather than that either the external or internal thread will strip. In other words, the length of thread engagement should be sufficient to develop the full strength of the screw. Thus, the length of internal thread and the dimensions of this thread, particularly its minor diameter, should be such that, taking into account a possible difference in strength of material of the internal and external threads, the threaded portion of the externally threaded part will break before either the external or internal threads strip. Due to this situation, lengths of engagement formulas are derived from shear formulas with tensile stress area As replaced by 2AS because the required area in shear is twice the tensile stress area in order to develop the full strength of the externally threaded part. This relationship is based upon experiments made by the National Bureau of Standards in 1929, in which it was found that for hot-rolled and cold-rolled steel, and brass screws and nuts, this factor varied from 1.7 to 2.0. The effect of combined stress is not taken into account in calculation of LE because the added shear load affects both tensile and shear stresses in approximately the same proportion.

70.7.2 All formulas for length of engagement, given in table II.B.2 yield approximate values since they are based in part upon shear areas which are not exact due to nut dilation which varies with geometry, friction forces, and material properties. Also, the effectiveness of partial threads, in the countersinks (or chamfers) on the ends of the internal thread, is not always the same. For calculations, approximately half the countersink depth may be considered in the length of engagement. It is advisable that calculations of length of engagement and corresponding load capabilities of a threaded joint be checked by actual tests, for critical joints.

70.7.3 When the externally and internally threaded parts are made from materials of approximately the same strength, required length of engagement in formula (13) of table II.B.2 may be applied. This assumes a combination failure of both threads. See 70.5.

70.7.4 When the strength of the internal thread materially exceeds that of the external thread, required length of engagement in formula (14) of table II.B.2 may be applied. This assumes shear of the external thread and uses the geometric shear area of the minimum external thread. See 70.2. A slightly longer or shorter length of engagement will be indicated if the simplified formula (5) in table II.B.1 is used.

70.7.5 When the strength of the external thread materially exceeds that of the internal thread, required length of engagement in formula (16) of table II.B.2 is used. This is based upon the internal thread stripping load being equal to the nominal external thread stripping load which will develop full strength of the externally threaded part. If  $R_1/R_2$  is less than 1, see 70.7.4 and if approximately equal to 1, see 70.7.3.

.70.7.6 For an adjusting or lead screw, or if the connection will be frequently unscrewed, the calculated LE should be increased to allow for the expected wear on the flanks of the threads during the useful life of the components.

70.7.7 For tapped holes in sheet metal, the maximum size of the screw to be specified should be such that the thickness of sheet equals the LE required to develop full strength. In order to use the largest possible screw, it is necessary that the tolerance,  $TD_1$ , on the minor diameter of the hole should be the practical minimum. If it should prove to be impracticable to reduce the minor diameter tolerance to such a value, it may be necessary to decrease the minimum minor diameter of the internal thread and to increase the minor diameter of the screw must be reduced by the same amount to prevent interference and the minor diameter of the screw. In all such cases, where dimensions are altered from those calculated according to the standard, the threads should be designated as specified in section 6.7 of ANSI B1.1-1982.



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70.7.8 For retaining collars on shafts where the expected axial force resisted by the collar is appreciably less than the tensile force that the shaft itself is capable of resisting, LE need only be long enough to withstand the expected axial force on the collar. If  $F_c$  is the axial force to be carried by the collar, UTS<sub>s</sub> is the tensile strength of the shaft and UTS<sub>n</sub> is the tensile strength of the collar, calculate the required length of engagement from one of the following formulas:

a. Collar thread strip: 
$$LE = \frac{2F_c}{UTS_n \times \frac{AS_n}{LE}}$$
 from (2a), (2b) or (3)

b. Shaft thread strip:  $LE = \frac{2F_c}{UTS_s \times AS_s}$  from (4a), (4b) or (5) LE

c. Combination thread stripping when UTS<sub>s</sub> = UTS<sub>n</sub> approximately:

$$LE = \frac{2F_{c}}{(UTS_{s} \text{ or } UTS_{n})x \underline{AS}_{s} \text{ from (7)}}$$
LE

Note: Numbers in parenthesis are formula numbers from table II.B.1.

70.7.9 For hollow, thin wall threaded parts as the wall thickness of either or both the internal and external members becomes thin, the tendency of the external member to enlarge and the internal member to neck down in the thread means that an LE greater than given by formula must be used, also that the tolerances on minor diameter of the internal thread and major diameter of the external thread,  $TD_1$  and Td, must be small to obtain the maximum practicable depth of thread engagement. For components having threads on thin-wall tubing, tests under actual working conditions should be made to determine proper selection of wall thicknesses, length of engagement, and pitch of thread.

80. Thread proportions in relation to tapping.

80.1 In the production of threads it is considered impractical to tap a thread unless its nominal diameter is greater than six times the basic thread height; therefore, when the ratio of D to h is less than 6, the use of a larger diameter, a finer pitch of thread, or both, should be considered.

80.2 The size of  $D_1$  is a factor in controlling tap breakage. Tap breakage is infrequent if the diameter of the tap is over 0.5 in or if the length of thread to be tapped is less than 0.5D. For sizes less than 0.5 in and length of thread over 0.5D, tap breakage can be minimized by use of a large  $D_1$ , that is  $TD_1$  maximum. However, this means that LE may have to be increased to develop the full strength of the screw.

# 90. Examples of thread design.

90.1 <u>Gun barrel thread.</u> A gun barrel is subjected to an internal explosive pressure that produces a tensile stress in the threaded end. The length of engagement of the threads should be sufficient to produce a minimum area in shear on the threads of the screw in line with the minor diameter of the tapped hole threads equal to twice the stress area of the threaded portion of the barrel. Assume that the thread on the barrel is 1.500-8UN-2A and the minimum internal diameter of the barrel at the threaded end is 0.792 inch.

Note: Symbol notation and formula numbers in parenthesis are in accordance with tables II.B.1 and II.B.2.

a. Required length of engagement is found using formula (14) for a hollow part.

 $LE = \frac{2(A_{s} - 0.7854 d_{h}^{2})}{3.1416 n D_{l}max \left[\frac{1}{2n} + 0.57735 (d_{2}min - D_{l}max)\right]}$ with  $A_{s} = 0.7854 (d_{bsc} - 0.9743)^{2}$ . In this case,  $A_{s}$  may be read as 1.492 from table 13 of ANSI B1.1-1982.  $d_{h} = 0.792$  n = 8  $D_{l}max = 1.390$  from table 3A of ANSI B1.1-1982  $d_{2}min = 1.4093$  from table 3A of ANSI B1.1-1982

b. Calculating from the above yields a required length of engagement of 0.777 inch. By reducing the internal thread minor diameter tolerance by half, the resulting  $D_1$  max is reduced to 1.3775 inches, and the required length of engagement is reduced to 0.714 inch.

90.2 Screws mounting bracket to cast iron part. The dimension is required for the largest steel cap screw that can be used to hold a bracket on a cast iron body. The tensile strength of the steel is 60,000 psi, the tensile strength of the cast iron 20,000 psi, and the thickness of the cast iron is such that the length of thread engagement cannot exceed 1.750 in. The screws on the top side of the bracket will be in tension.

Note: Symbol notation and formula numbers in parenthesis are in accordance with tables II.B.1 and II.B.2.

- a. Since the external thread material is considerably stronger than that of the internal thread material, in accordance with 70.7.5, formula (16) will be used to calculate the length of engagement required. This formula is applied for LE based upon shear of the internal thread. To confirm this assumption,  $R_1/R_2$  should be calculated.
- b.  $R_1$  cannot be calculated from formula (8) until a thread size is selected. By definition, however,  $R_1$  is the ratio of external thread shear area to internal thread shear area. An approximation of  $R_1$ , can be made by using the simplified formulas for shear areas so

Approximate 
$$R_1 = \frac{Formula(5)}{Formula(3)} = 0.833$$

c. R<sub>2</sub> is calculated from formula (9).

$$R_2 = \frac{UTS_n}{UTS_n} = \frac{20000}{60000} = 0.333$$

- d. From b and c above,  $R_1/R_2 = 2.5$  approximately. This value being greater than 1 confirms the use of formula (16) for calculation of length of engagement.
- e. From formula (16) it is seen that the length of engagement must be approximately 2.5 times as long as that required if shear in the external thread were the controlling factor. Thus, since the maximum available LE is 1.750 inches, the approximate LE required for the screw to develop full strength is 1.750/2.5 = 0.700 inch.
- f. Inasmuch as the hole is tapped in cast iron, a relatively coarse thread would be required, that is UNC or coarser. The most readily available screws would be UNC. Select thread sizes from figure 2.B.2 which yield LE of approximately 0.700 inch. Figure 2.B.2 was developed from formula (15).

For 1"-8UNC, LE/D=0.594 and LE=0.594

For  $1\frac{1}{8}$  -7UNC, LE/D = 0.592 (est.) and LE = 0.656

For  $1\frac{1}{4}$  - 7UNC, LE/D = 0.600 (est.) and LE = 0.750

- g. For a bracket screw, the preferred thread class is 2A so the selected thread is  $1\frac{1}{8}$  -7UNC-2A for the cap screw. The corresponding hole in the body would have a  $1\frac{1}{8}$  -7UNC-2B thread.
- h. The thread should be checked in accordance with formula (16). Formula (16) may be expressed as follows:

$$LE = \frac{2 A_s}{3.1416 D_l \min x \frac{3}{4}} \times \frac{R_l}{R_2}$$

with  $A_s = 0.7854 \left( d_{bsc} - \frac{0.9743}{n} \right)^2$ . In this case,  $A_s$  may be read as 0.763 from table 8 of ANSI B1.1 - 1982.

 $D_1 min = 0.970$  from table 3A of ANSI B1.1 - 1982.

$$R_{1} = \frac{Formula(6b)}{Formula(2a)} = \frac{\frac{3}{4} \times D_{1}min}{n dmin \left[\frac{1}{2n} \times 0.57735 (dmin - D_{2}max)\right]}$$
$$n = 7$$

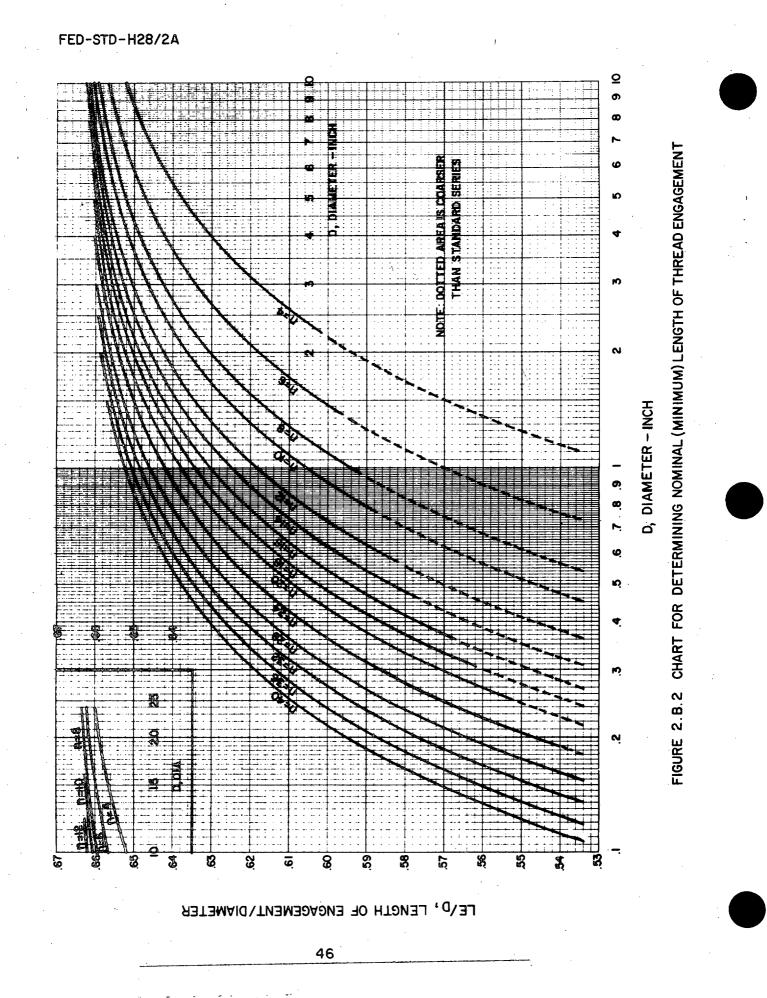
dmin = 1.1064 from table 3A of ANSI B1.1-1982

D<sub>2</sub>max = 1.0416 from table 3A of ANSI B1.1-1982

so 
$$R_1 = 0.863$$

 $R_2 = 0.333$  from c above.

i. Calculating from the above yields a required length of engagement of 1.729 inches. This is acceptable since it is less than the maximum available engagement length of 1.750.



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	NDARDIZATION DOCUMENT I (See Instructions - R	
1. DOCUMENT NUMBER FED-STD-H28/2A 30. NAME OF SUBMITTING ORG	2. DOCUMENT TITLE Unified Inch Screw Thr ANIZATION	eads-UN and UNR Thread Forms
b. ADDRESS (Street, City, State, 2	IP Code)	USER MANUPACTURER OTHER (Spec(ly));
5. PROBLEM AREAS a. Peregreph Number end Wordir	•:	
ö. Recommended Wording:		
c. Resson/Rationals for Recomm	rendstion:	
REMARKS	********	
NAME OF SUBMITTER (Last, P		b. WORK TELEPHONE NUMBER (Include Area Code) - Optional 8. DATE OF SUBMISSION (YYMMDD)
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